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## Chapter 2 - Fourier optics and imaging

# Course contents



**Cover the unifying concepts of imaging, including with electrons, optics, X-rays. In 2D, 3D, and beyond.**

## **Chapter 1 Interactions of waves with the sample and beyond**

- Review of Fourier transform and properties
- Helmholtz equation
- Angular spectrum and evanescent waves
- Huygens–Fresnel principle
- Rayleigh-Sommerfeld solution
- Fresnel approximation
- Fraunhofer approximation – the far field
- Paraxial wave equation
- Projection approximation
- Multislice propagation
- Beer-Lambert law

# Recap on propagation

Angular spectrum

$$U(x, y, z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \{ U(x, y, 0) \} H(f_x, f_y) \right\}$$

$$H(f_x, f_y) = \exp \left[ i 2 \pi z \sqrt{\left( \frac{k_0}{2\pi} \right)^2 - f_x^2 - f_y^2} \right]$$

Rayleigh-Sommerfeld

$$U(P_0) = U(P_1) * h(x_1, y_1)$$

$$h(x, y) = \frac{1}{i\lambda_0} \left( 1 - \frac{1}{ik_0 r} \right) \frac{\exp(ikr)}{r} \frac{z}{r}$$

# Fresnel approximation

Convolution form

$$U_o(x, y) = U_i(x, y) * h(x, y)$$

$$h(x, y) = \frac{\exp(ik_0z)}{i\lambda_0z} \exp\left(\frac{ik_0}{2z}[x^2 + y^2]\right)$$

$$\tilde{U}_0(f_x, f_y) = \tilde{U}_i(f_x, f_y) H(f_x, f_y)$$

$$H(f_x, f_y) = \exp(ik_0z) \exp\left[-i\pi\lambda_0z(f_x^2 + f_y^2)\right]$$

Single Fourier transform form

$$U_o(x, y) = \frac{\exp(ik_0z)}{i\lambda_0z} \exp\left[\frac{ik_0}{2z}(x^2 + y^2)\right] \mathcal{F} \left\{ U_i(\xi, \eta) \exp\left[\frac{ik_0}{2z}(\xi^2 + \eta^2)\right] \right\} \begin{matrix} f_x = \frac{x}{\lambda_0z} \\ f_y = \frac{y}{\lambda_0z} \end{matrix}$$

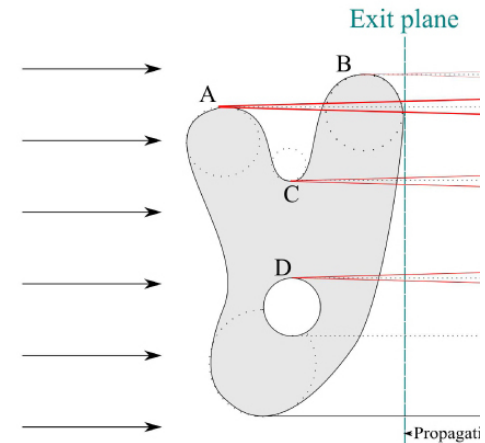
# Projection approximation

The object is thin enough, and boring enough, that we can ignore any diffraction within it

$$\tilde{\psi}(x, y, z = z_1) \approx \tilde{\psi}(x, y, z = z_0) o(x, y)$$

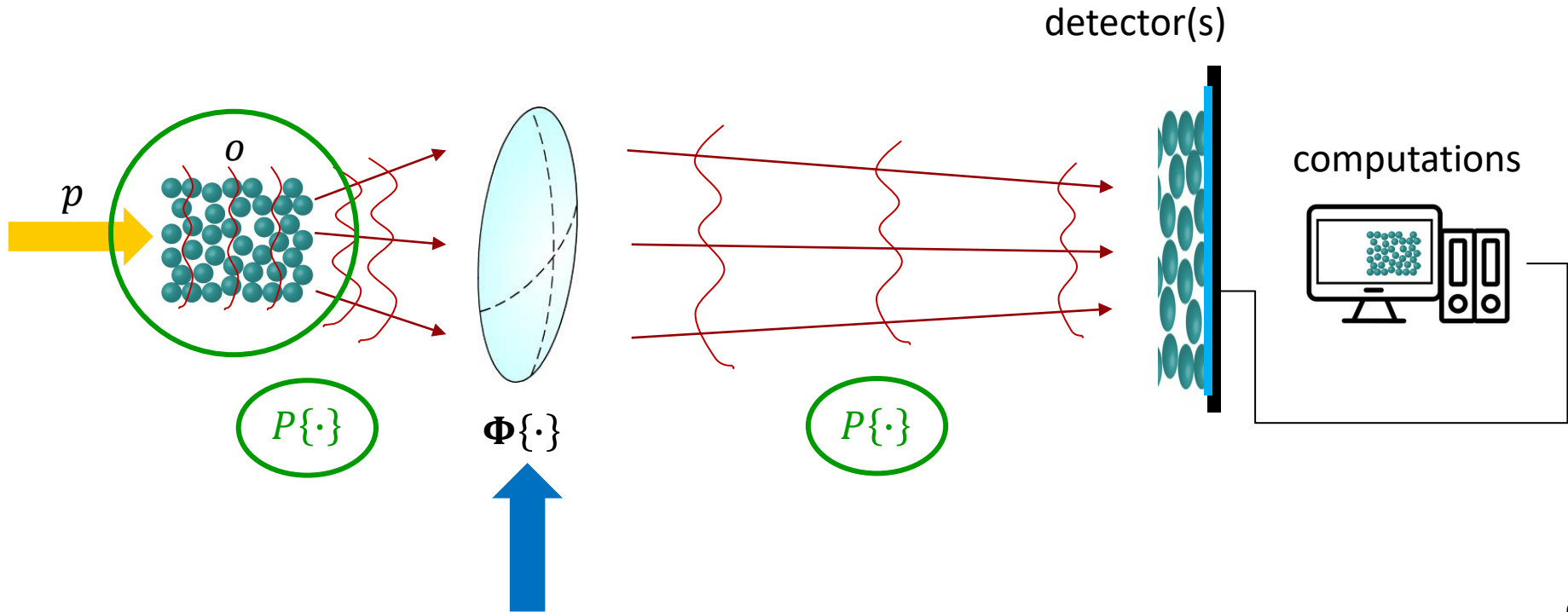
$$o(x, y) = \exp(ik_0 z) \exp\left\{ik_0 \int_0^z [n(x, y, z) - 1] dz\right\}$$

$n = 1 - \delta + i\beta$   
Index of refraction is complex-valued



# Lenses and imaging

A more detailed model



# Course contents

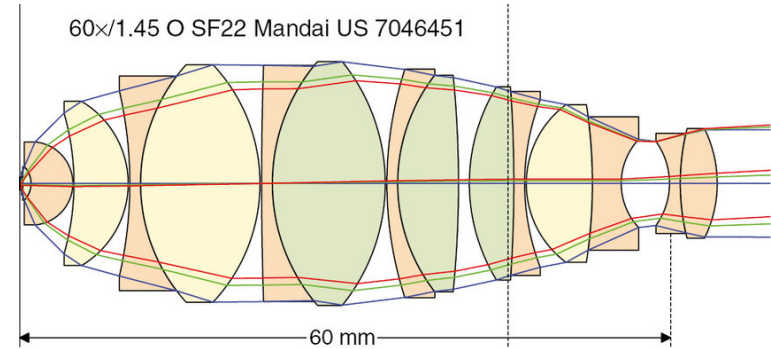
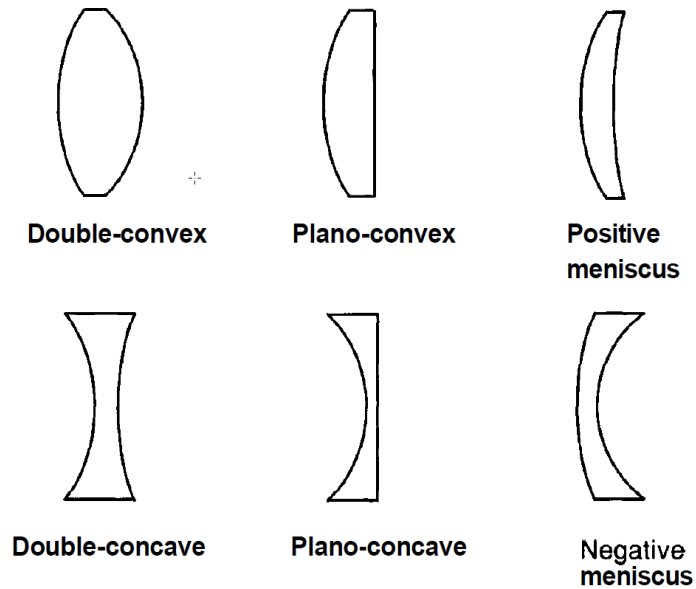
**Cover the unifying concepts of imaging, including with electrons, optics, X-rays.  
In 2D, 3D, and beyond.**

## **Chapter 2 - Fourier Optics and Imaging**

- Lens transmissivity
- Fourier transforming properties of lenses
- Focused beams
- Imaging
- Frequency response of optical systems (coherent and incoherent cases)
- Wavefront aberrations
- Propagation through complicated paraxial optical systems

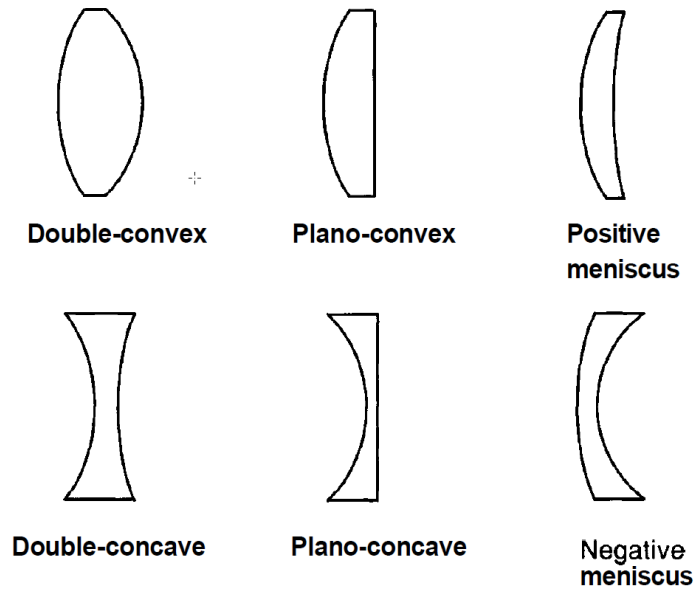
**Lens transmissivity**

# Types of lenses



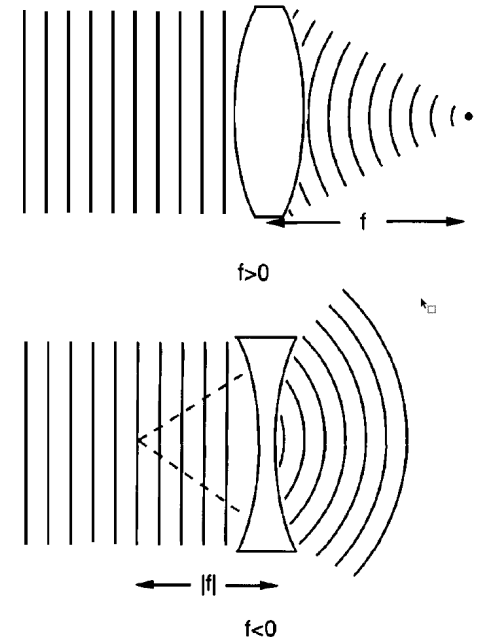
**FIGURE 5.3**  
Various types of lenses.

# Types of lenses



**FIGURE 5.3**  
Various types of lenses.

$\text{Re}\{n\} > 1$



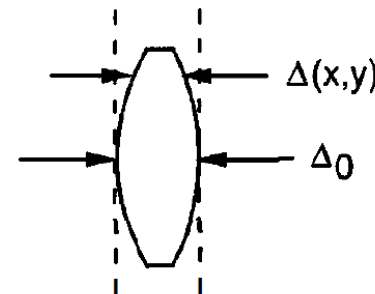
# The thin lens transmissivity

Projection approximation (thin lens)

$$t_l(x, y) = \exp(\cancel{ik_0\Delta_0}) \exp\left\{ik_0 \int_{z_0}^{z_1} [n(x, y, z) - 1] dz\right\}$$

$$n = 1 - \delta + i\beta$$

Index of refraction is complex-valued



$$t_l(x, y) = \exp\{ik_0 \text{OPD}(x, y)\} = \exp\{i\phi(x, y)\}$$

$$\phi = k_0 \int_{z_0}^{z_1} [n(x, y, z) - 1] dz$$

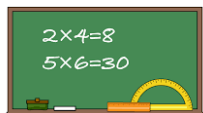
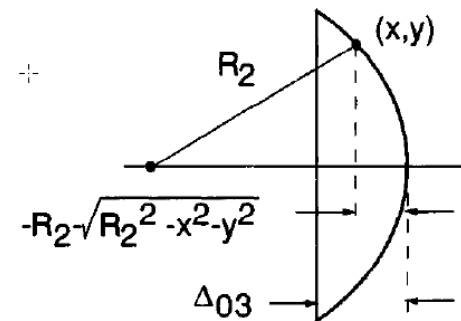
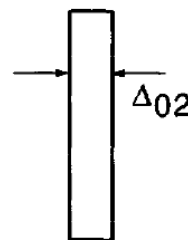
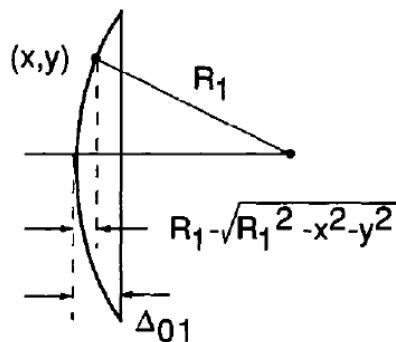
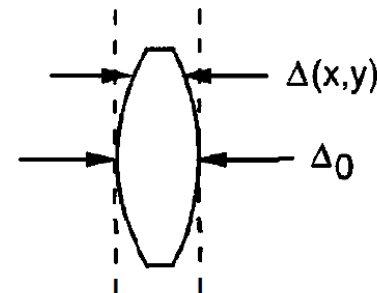
$$\phi = k_0 \int_{z_0}^{z_1} [n(x, y, z) - 1] dz = k_0(n - 1)\Delta(x, y)$$

Note it is different from Goodman's by the constant phase factor.

# The thin lens transmissivity

$$U'_l(x, y) = t_l(x, y)U_l(x, y)$$

$$t_l(x, y) = \exp\{ik_0(n-1)\Delta(x, y)\}$$



# The thin lens transmissivity

Paraxial approximation

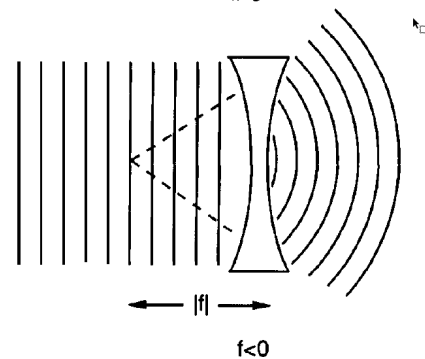
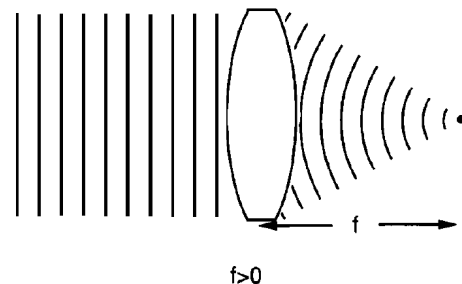
$$\Delta(x, y) = \Delta_0 - \frac{x^2 + y^2}{2} \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$$

$$t_l(x, y) = \exp \{ ik_0 (n-1) \Delta(x, y) \}$$

Lens-maker equation for a thin lens

$$\frac{1}{f} \approx (n-1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$$

$$t_l(x, y) = \exp \left\{ -\frac{ik_0}{2f} (x^2 + y^2) \right\}$$



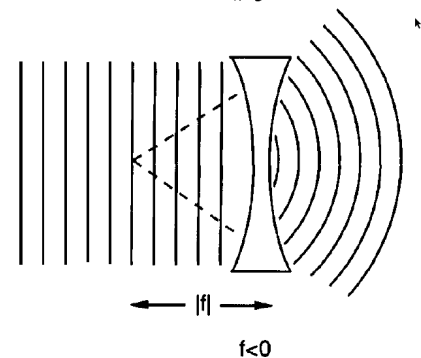
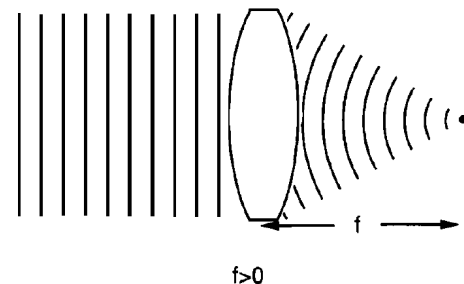
# The thin lens transmissivity

For input plane wave

$$U_l'(x, y) = \exp\left\{-\frac{ik_0}{2f}(x^2 + y^2)\right\} \cdot 1$$

Point source in Fresnel approximation

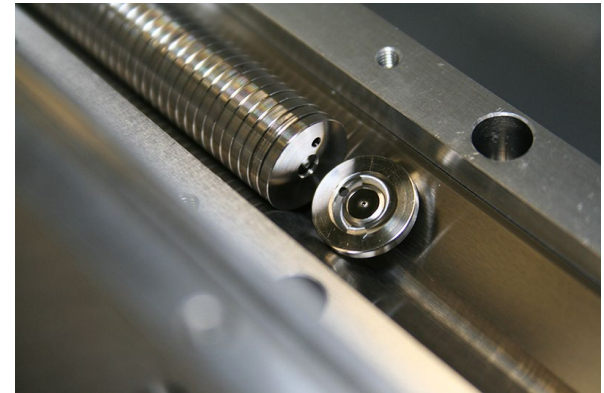
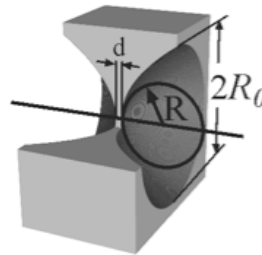
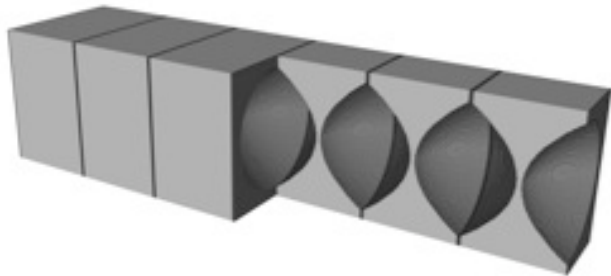
$$h(x, y) = \frac{\exp(ik_0z)}{i\lambda_0z} \exp\left(\frac{ik_0}{2z}[x^2 + y^2]\right)$$



# Side note for X-rays

Phase velocity of the wave is larger than  $c$   
X-ray compound refractive lenses

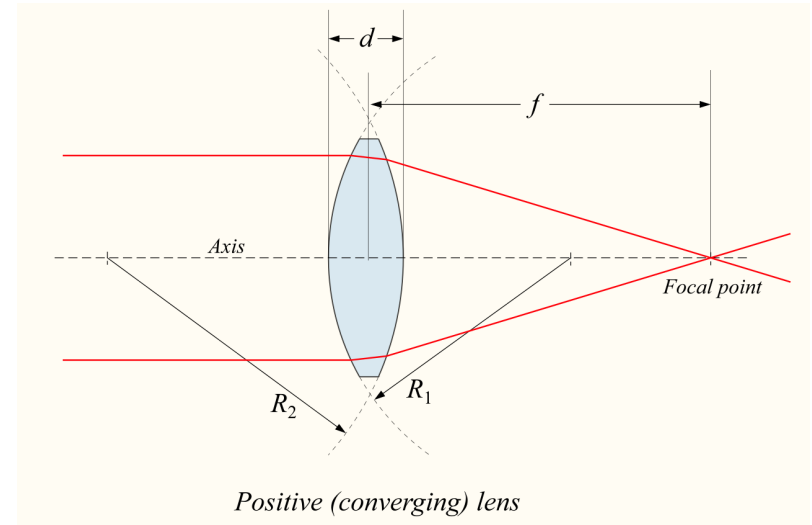
$$\text{Re}\{n\} < 1$$



Stack of beryllium compound refractive lenses

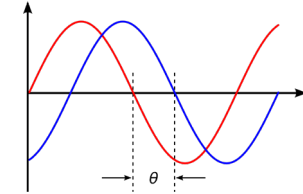
# Side note for thick lenses

$$\frac{1}{f} = (n-1) \left[ \frac{1}{R_1} - \frac{1}{R_2} + \frac{(n-1)d}{nR_1R_2} \right]$$

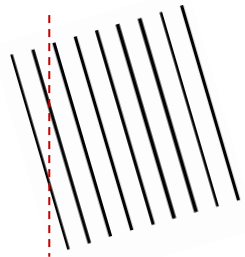


# Phase of a wavefield

Phase differences describe relative offset of waves



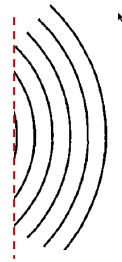
Represent wavefields by lines of constant phase



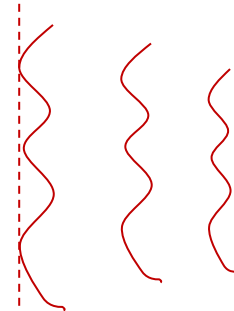
Plane-wave



Converging

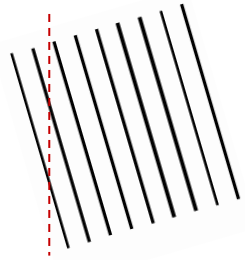


Diverging



Miscellaneous

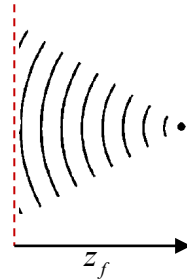
# Phase of a wavefield



Plane-wave

$$U(x, y) = A \exp[i(k_x x + k_y y)]$$

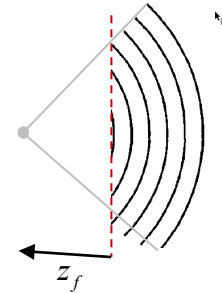
Linear phase



Converging

$$U_o(x, y) = \exp\left[-\frac{ik_0}{2z_f}(x^2 + y^2)\right]$$

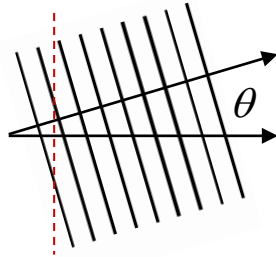
Quadratic phase



Diverging

$$U_o(x, y) = \exp\left[\frac{ik_0}{2z_f}(x^2 + y^2)\right]$$

# Local derivative of the phase

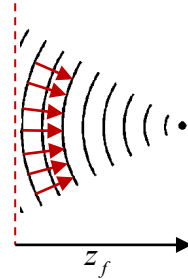


Plane-wave

$$U(x, y) = A \exp[i(k_x x + k_y y)]$$

$$\frac{\partial \phi}{\partial y} = k_x = \frac{2\pi}{\lambda} \sin \theta$$

$$\sin \theta = \frac{\lambda}{2\pi} \frac{\partial \phi}{\partial y}$$



Converging

$$U_o(x, y) = \exp\left[-\frac{ik_0}{2z_f}(x^2 + y^2)\right]$$

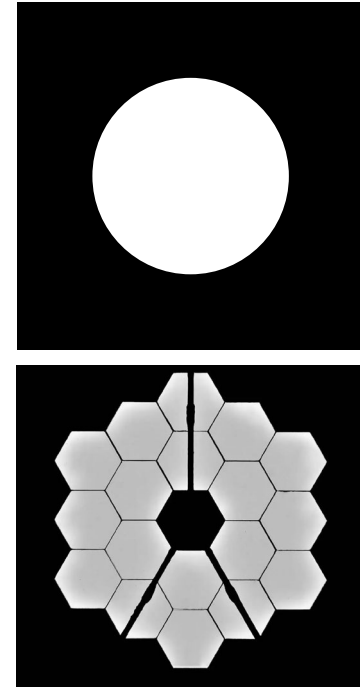
$$\sin \theta = \frac{\lambda}{2\pi} \frac{\partial}{\partial y} \left[-\frac{k_0}{2z_f}(x^2 + y^2)\right] = -\frac{x}{z_f}$$

# The aperture

Account for the limited physical extent of the lens via a pupil function

$$t_l(x, y) = P(x, y) \exp \left\{ -\frac{ik_0}{2f} (x^2 + y^2) \right\}$$

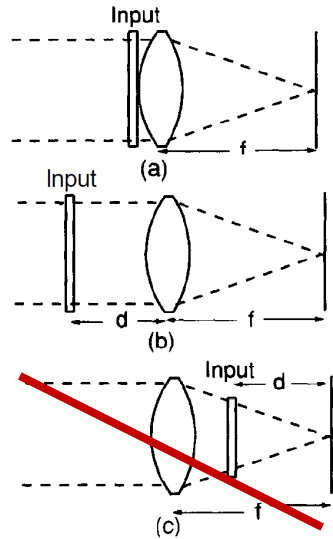
$$P(x, y) = \begin{cases} 1 & \text{inside the lens aperture} \\ 0 & \text{otherwise} \end{cases}$$



# **Fourier transforming properties of lenses**

# Fourier transform using a lens

One of the most remarkable and useful properties of a converging lens is its inherent ability to perform two-dimensional Fourier transforms. This complicated analog operation can be performed with extreme simplicity in a coherent optical system, taking advantage of the basic laws of propagation and diffraction of light.

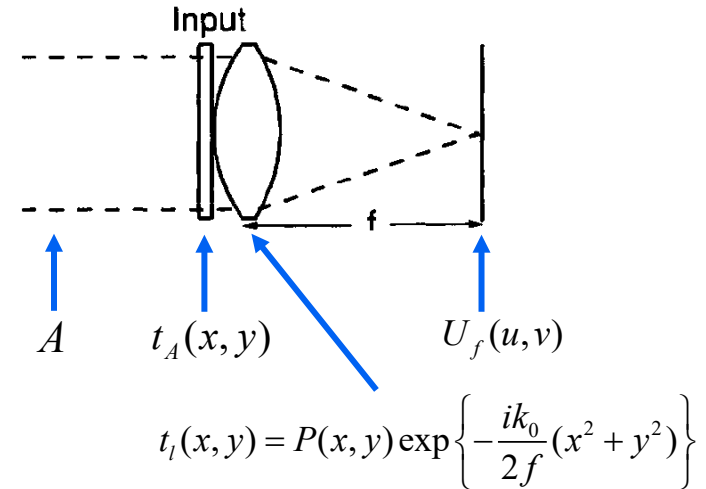


**FIGURE 5.5**

Geometries for performing the Fourier transform operation with a positive lens.

# Fourier transform using a lens case (a)

Object directly against the lens

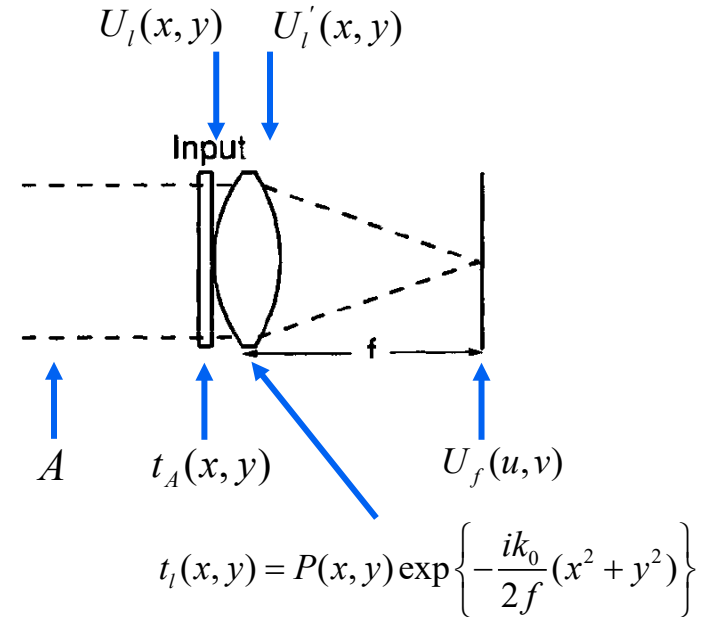


# Fourier transform using a lens case (a)

Object directly against the lens

$$U_f(u, v) = \frac{A}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} \mathcal{F}\{t_A(x, y)P(x, y)\} \begin{matrix} f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f} \end{matrix}$$

$$U_f(u, v) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} \mathcal{F}\{U_l(x, y)P(x, y)\} \begin{matrix} f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f} \end{matrix}$$

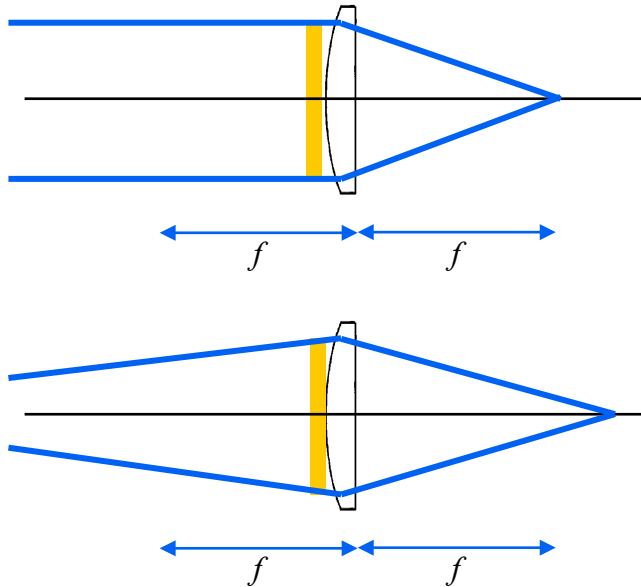


**Focused beams**



# Focused beams

No object corresponds to focusing a beam  $\rightarrow$  Beam at focus is the FT of the pupil



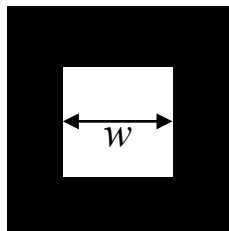
# The focused beam – square aperture

Beam at the focus will be equal to the FT of the pupil  $t_A(x, y) = 1$

$$U_f(u, v) = \frac{A}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} \mathcal{F}\{t_A(x, y)P(x, y)\}_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$

For square pupil

$$P(x, y) = \text{rect}\left(\frac{x}{w}\right) \text{rect}\left(\frac{y}{w}\right)$$



$$\mathcal{F}\{P(x, y)\} = w^2 \text{sinc}(wf_x) \text{sinc}(wf_y)$$

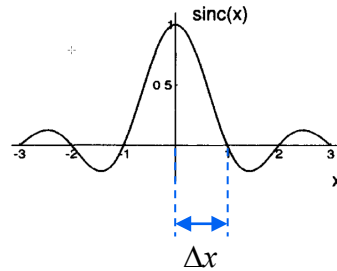
$$U_f(u, v) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} w^2 \text{sinc}\left(\frac{wu}{\lambda f}\right) \text{sinc}\left(\frac{wv}{\lambda f}\right)$$

# The focused beam – square aperture

For square pupil  $P(x, y) = \text{rect}\left(\frac{x}{w}\right) \text{rect}\left(\frac{y}{w}\right)$

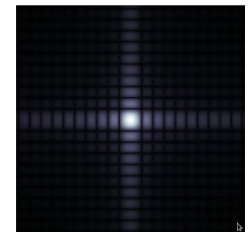
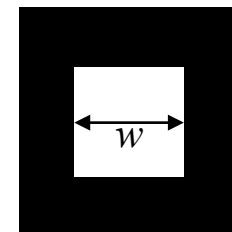
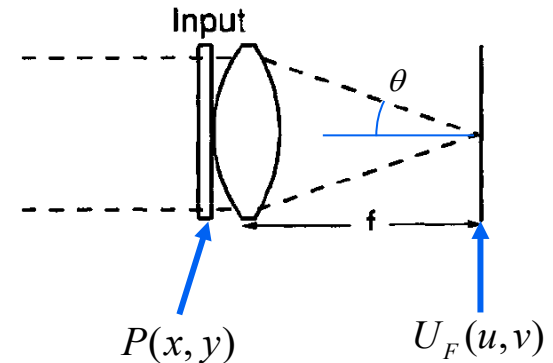
$$U_f(u, v) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} w^2 \text{sinc}\left(\frac{wu}{\lambda f}\right) \text{sinc}\left(\frac{wv}{\lambda f}\right)$$

$$\text{sinc}(x) = \frac{\sin(\pi x)}{\pi x}$$



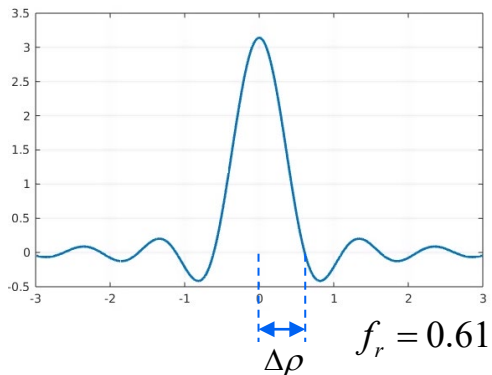
$$\frac{w\Delta x}{\lambda f} = 1$$

$$\Delta x = \frac{\lambda f}{w} = \frac{\lambda}{2 \tan(\theta)} \approx \frac{\lambda}{2 \sin(\theta)}$$



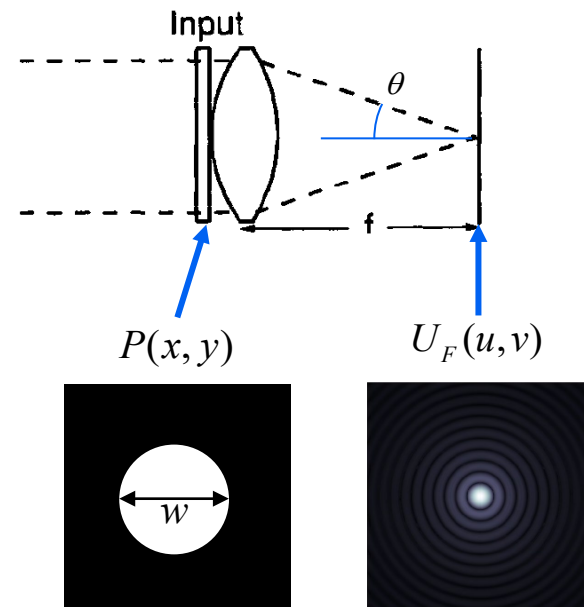
# The focused beam – circular aperture

Circular pupil  $\mathcal{F}\{\text{circ}(r)\} = 2\pi \frac{J_1(2\pi f_r)}{(2\pi f_r)} \quad (2-36)$



$$\frac{w}{2} \frac{\rho}{\lambda f} = 0.61$$

$$\Delta\rho = 1.22 \frac{\lambda f}{w} = \frac{0.61\lambda}{\tan(\theta)} \approx \frac{0.61\lambda}{\sin(\theta)}$$



# Many names for this one

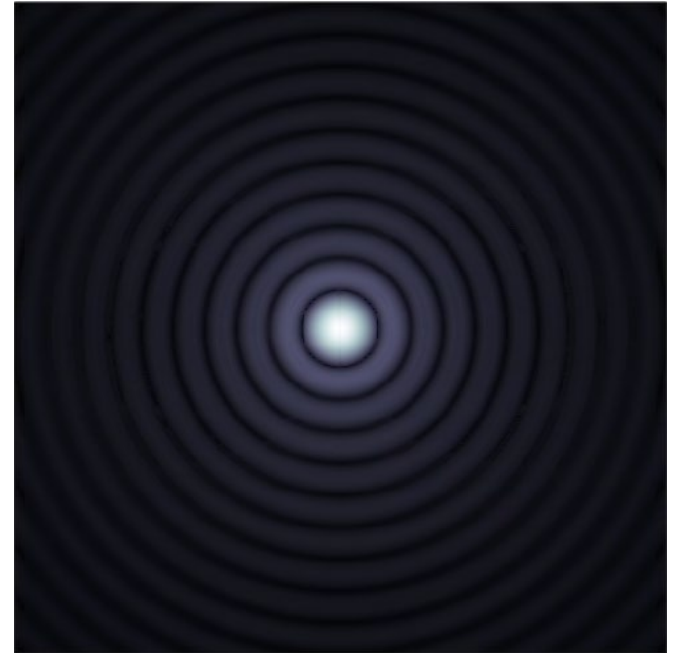
Besinc

Jinc

Sombrero function (?)

Airy disk (if squared)

$$h(\rho) = 2\pi \frac{J_1\left(2\pi \frac{w}{2} \frac{\rho}{\lambda f}\right)}{\left(2\pi \frac{w}{2} \frac{\rho}{\lambda f}\right)}$$



# **Fourier transforming properties of lenses**

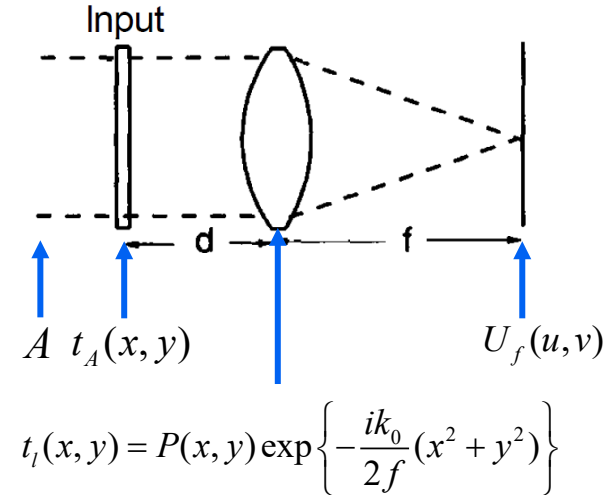
# Fourier transform using a lens case (b)

$$U_f(u, v) = \mathcal{P}_f \left\{ \mathcal{P}_d \left\{ At_A(x, y) \right\} t_l(x, y) \right\}$$

$$U_l(x, y) = \mathcal{P}_d \left\{ At_A(x, y) \right\} = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ At_A(x, y) \right\} \exp \left( -i\pi\lambda d \left[ f_x^2 + f_y^2 \right] \right) \right\}$$

$$U_f(u, v) = \frac{1}{i\lambda f} \exp \left\{ \frac{ik_0}{2f} (u^2 + v^2) \right\} \mathcal{F} \left\{ U_l(x, y) P(x, y) \right\} \Bigg|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$

$$U_f(x, y) = \frac{1}{i\lambda f} \exp \left\{ \frac{ik_0}{2f} (u^2 + v^2) \right\} \mathcal{F} \left\{ At_A(x, y) \right\} \exp \left( -i\pi\lambda d \left[ f_x^2 + f_y^2 \right] \right) \Bigg|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$



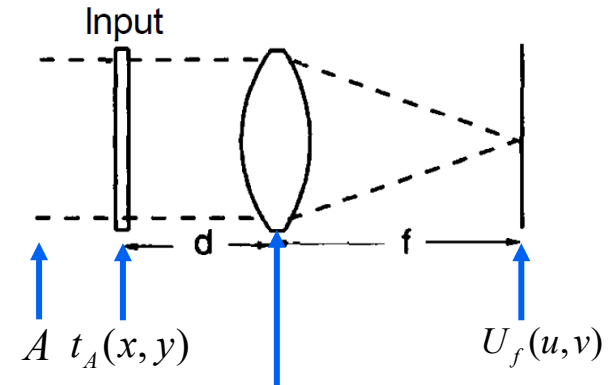
# Fourier transform using a lens case (b)

$$U_f(x, y) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} \mathcal{F}\{At_A(x, y)\} \exp\left(-i\pi\lambda d[f_x^2 + f_y^2]\right) \Bigg|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$

# Fourier transform using a lens case (b)

$$U_f(x, y) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\right\} \mathcal{F}\{At_A(x, y)\} \exp\left(-i\pi\lambda d\left[f_x^2 + f_y^2\right]\right) \Big|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$

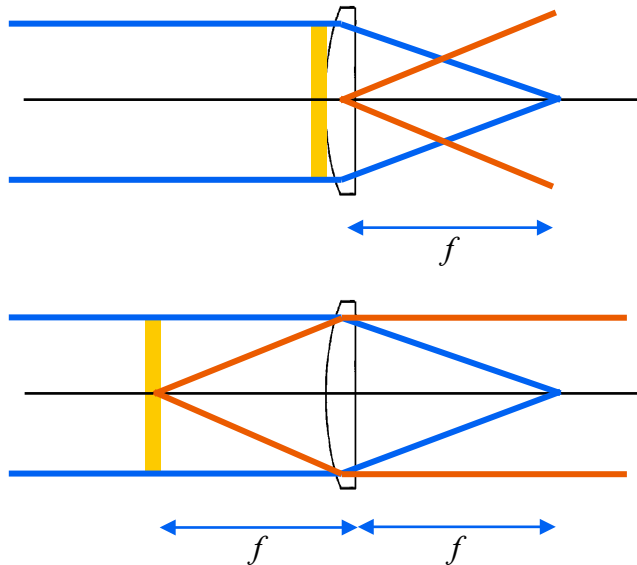
$$U_f(x, y) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\left(1 - \frac{d}{f}\right)\right\} \mathcal{F}\{At_A(x, y)\} \Big|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$



$$t_l(x, y) = P(x, y) \exp\left\{-\frac{ik_0}{2f}(x^2 + y^2)\right\}$$

# The external quadratic factor to the FT

$$U_f(x, y) = \frac{1}{i\lambda f} \exp \left\{ \frac{ik_0}{2f} (u^2 + v^2) \left( 1 - \frac{d}{f} \right) \right\} \mathcal{F} \{ At_A(x, y) \} \Big|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$

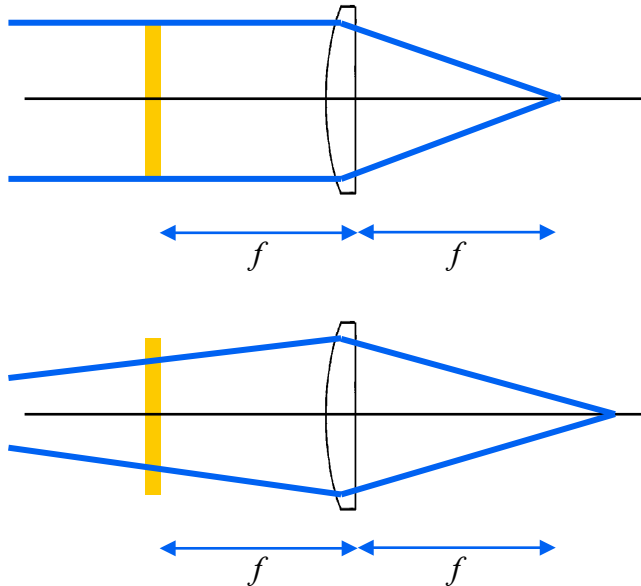


The quadratic phase corresponds to that obtained if the object was a point source

While it is not obvious without some further thought and analysis, our results show that the quadratic-phase factor preceding the Fourier transform operation is always the quadratic-phase factor that would result at the transform plane from a point source of light located on the optical axis in the plane of the input transparency.

# The location of the Fourier planes

$$U_f(x, y) = \frac{1}{i\lambda f} \exp\left\{\frac{ik_0}{2f}(u^2 + v^2)\left(1 - \frac{d}{f}\right)\right\} \mathcal{F}\{At_A(x, y)\} \Big|_{\substack{f_x = \frac{u}{\lambda f} \\ f_y = \frac{v}{\lambda f}}}$$



The Fourier transform plane need not be the focal plane of the lens performing the transform!  
Rather, the Fourier transform always appears in the plane where the source is imaged.

# Course contents

**Cover the unifying concepts of imaging, including with electrons, optics, X-rays.  
In 2D, 3D, and beyond.**

## **Chapter 2 - Fourier Optics and Imaging**

- Lens transmissivity
- Fourier transforming properties of lenses
- Focused beams
- Imaging
- Frequency response of optical systems (coherent and incoherent cases)
- Wavefront aberrations
- Propagation through complicated paraxial optical systems

**Imaging**

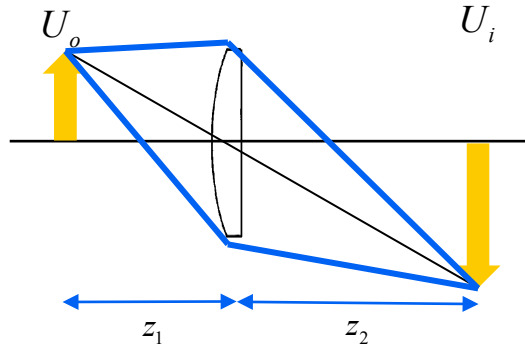


# What is imaging?

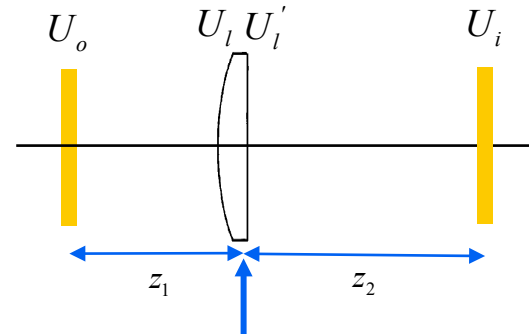
Mapping 1 to 1 between input and output plane

Some magnification is useful

There can be some distortion and/or blurring



# Imaging



$$t_l(x, y) = P(x, y) \exp \left\{ -\frac{ik_0}{2f} (x^2 + y^2) \right\}$$

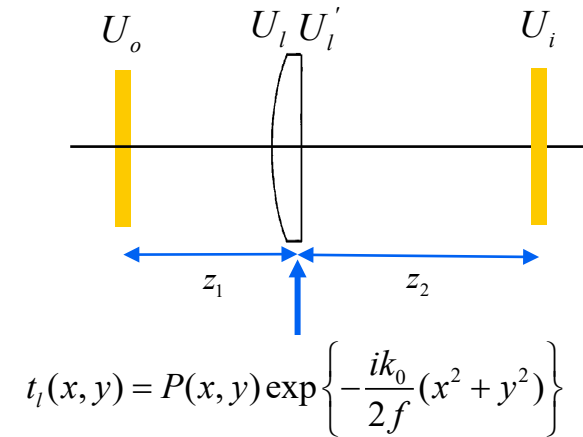
Note the derivation is different than Goodman's

# Imaging

$$U_i(x, y) = \exp\left(\frac{ik}{2z_2}[x^2 + y^2]\right) \left[ \frac{1}{|M|} U_o\left(\frac{x}{M}, \frac{y}{M}\right) \exp\left(\frac{ik}{2z_1 M^2}[x^2 + y^2]\right) \right] * h(x, y)$$

$$M = -\frac{z_2}{z_1}$$

$$h(x, y) = \frac{1}{M \lambda z_1 z_2} \mathcal{F}\{P(x_l, y_l)\} \quad \begin{matrix} f_x = \frac{x}{\lambda z_2} \\ f_y = \frac{y}{\lambda z_2} \end{matrix}$$



Object – Image are related by magnification and inversion

Effect of diffraction is convolution with an impulse response function  $h(x, y)$

Impulse response can blur fine details, it is actually like a low-pass filter

For most practical applications the quadratic factors are not important – but for phase imaging they do appear

# Frequency response of an optical system

Coherent case

# Frequency response of an optical system

All diffraction effects can be associated with either of these two pupils

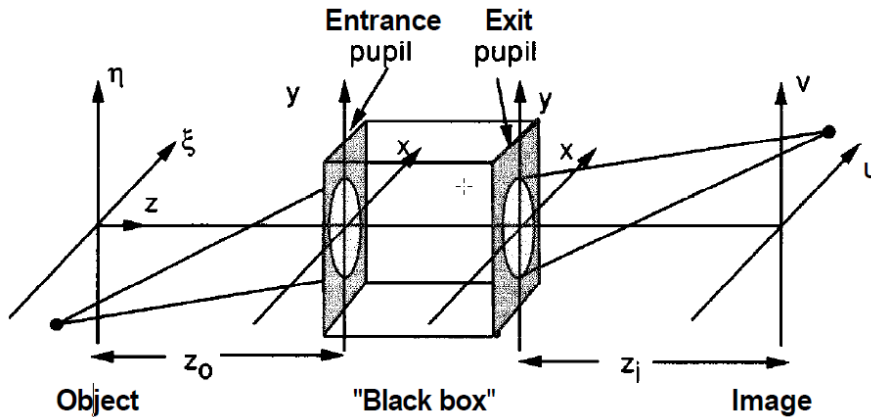
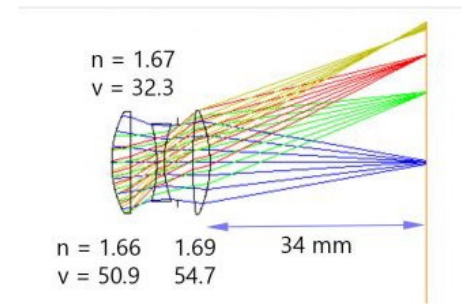
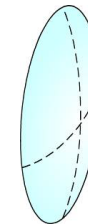


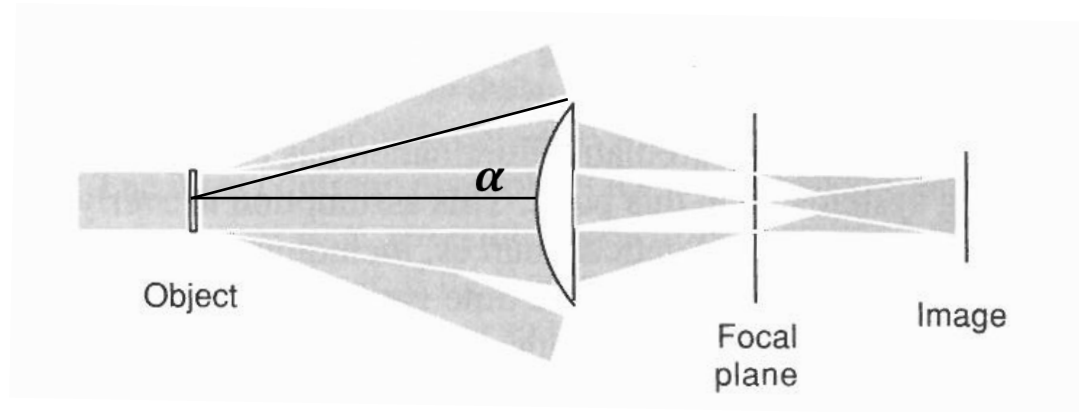
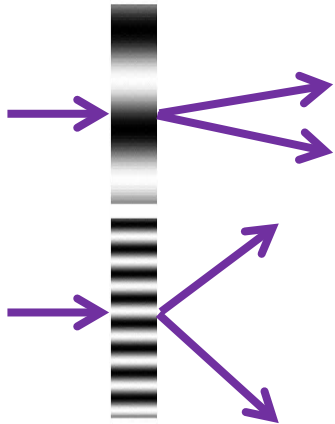
FIGURE 6.1  
Generalized model of an imaging system.



# Frequency response of an optical system

## Coherent case

Abbe theory of image formation  
High-resolution = high diffraction angles



Rayleigh resolution

$$\Delta x = \frac{0.61\lambda}{n \sin \alpha}$$

# Frequency response of an optical system

## Coherent case

Real space

Coherent → when light appears to come from a single point

$$U_i(x, y) = \exp\left(\frac{ik}{2z_2}[x^2 + y^2]\right) \left[ \frac{1}{|M|} U_o\left(\frac{x}{M}, \frac{y}{M}\right) \exp\left(\frac{ik}{2z_1 M^2}[x^2 + y^2]\right) \right] * h(x, y)$$

$$U_g(x, y) = \frac{1}{|M|} U_o\left(\frac{x}{M}, \frac{y}{M}\right) \exp\left(\frac{ik}{2z_1 M^2}[x^2 + y^2]\right)$$

$$h(x, y) = \frac{1}{M \lambda z_1 z_2} \mathcal{F}\{P(x_l, y_l)\}$$

$f_x = \frac{x}{\lambda z_2}$   
 $f_y = \frac{y}{\lambda z_2}$

$$U_i(x, y) = U_g(x, y) * h(x, y)$$

# Frequency response of an optical system

## Coherent case

Real and reciprocal space

$$U_i(x, y) = U_g(x, y) * h(x, y)$$

$$H(f_x, f_y) = \mathcal{F}\{h(x, y)\} = \mathcal{F}\left\{\frac{1}{\lambda^2 z^2} \iint P(x, y) \exp\left(-i \frac{2\pi}{\lambda z_i} [ux + vy]\right) dx dy\right\} = P(-\lambda z_i f_x, -\lambda z_i f_y)$$

$$\mathcal{F}\{U_i(x, y)\} = \mathcal{F}\{U_g(x, y)\} P(-\lambda z_i f_x, -\lambda z_i f_y)$$

# Circular pupil

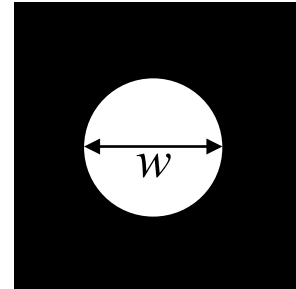
Exit pupil diameter

$$P(x, y) = \text{circ}\left(\frac{r}{w/2}\right)$$

$$H(x, y) = \text{circ}\left(\frac{\lambda z_i f_r}{w/2}\right)$$

Coherent transfer function

$$f_c = \frac{1}{2} \frac{w}{\lambda z_i} \quad \text{Cutoff frequency (w is exit pupil diameter)}$$



# Frequency response of an optical system

Incoherent case

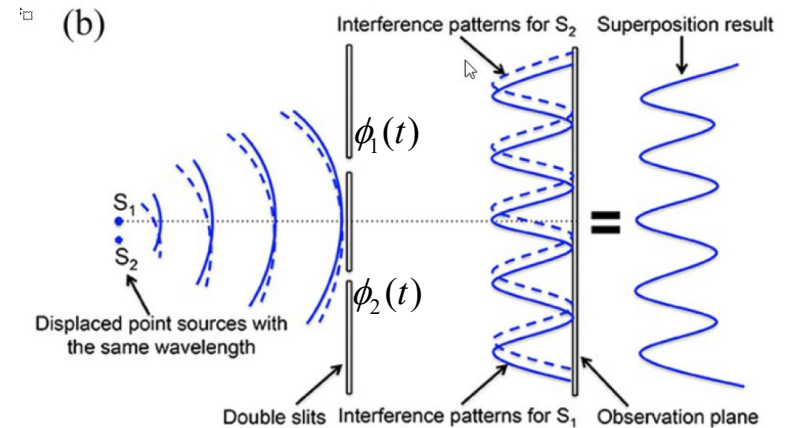
# About coherence and incoherence

Statistical property of light

$$I = \left\langle \cos^2 \left( \frac{2\pi x}{\tau} + \frac{\Delta\phi(t)}{2} \right) \right\rangle_t = \frac{1}{2} + \frac{1}{2} \left\langle \cos \left( \frac{2\pi x}{\tau/2} + \Delta\phi(t) \right) \right\rangle_t$$

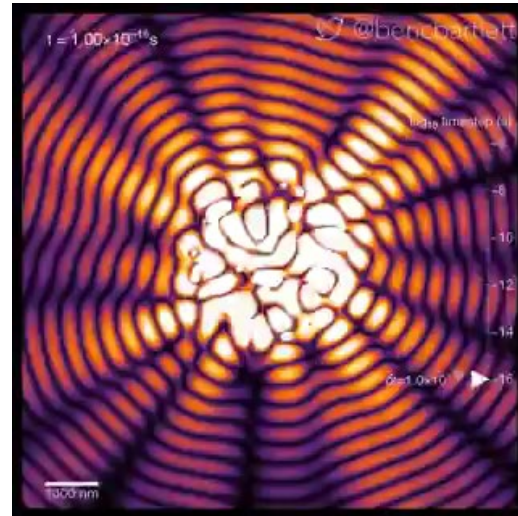
If phase difference is constant fringe visibility will be 1

If phase difference is completely random fringe visibility will be 0



# About coherence and incoherence

Thermal sources or vibrations much faster than the integration time



# Image intensity

For incoherent or partially coherent fields only intensity measurements averaged over time make sense

$$I_i(u, v) = \left\langle |U_i(u, v; t)|^2 \right\rangle$$
$$= \iint d\xi_1 d\eta_1 \iint d\xi_2 d\eta_2 h(u - \xi_1, v - \eta_1) h(u - \xi_2, v - \eta_2) \left\langle U_g(\xi_1, \eta_1; t - \tau_1) U_g^*(\xi_2, \eta_2; t - \tau_2) \right\rangle$$

Taking into account a small-area  $h(u, v)$  over which the time differences are small we can drop the time-delay difference

$$I_i(u, v) = \iint d\xi_1 d\eta_1 \iint d\xi_2 d\eta_2 h(u - \xi_1, v - \eta_1) h(u - \xi_2, v - \eta_2) J_g(\xi_1, \eta_1; \xi_2, \eta_2)$$
$$J_g(\xi_1, \eta_1; \xi_2, \eta_2) = \left\langle U_g(\xi_1, \eta_1; t) U_g^*(\xi_2, \eta_2; t) \right\rangle$$

= **mutual intensity** = measure of spatial coherence

# Incoherent imaging

Fields uncorrelated (for distances greater than  $\lambda$ )

$$I_i(u, v) = \iint d\xi_1 d\eta_1 \iint d\xi_2 d\eta_2 h(u - \xi_1, v - \eta_1) h(u - \xi_2, v - \eta_2) J_g(\xi_1, \eta_1; \xi_2, \eta_2)$$

$$J_g(\xi_1, \eta_1; \xi_2, \eta_2) = \langle U_g(\xi_1, \eta_1; t) U_g^*(\xi_2, \eta_2; t) \rangle$$

$$\langle U_g(\tilde{\xi}_1, \tilde{\eta}_1; t) U_g^*(\tilde{\xi}_2, \tilde{\eta}_2; t) \rangle = \kappa I_g(\tilde{\xi}_1, \tilde{\eta}_1) \delta(\tilde{\xi}_1 - \tilde{\xi}_2, \tilde{\eta}_1 - \tilde{\eta}_2)$$

Take square magnitude and convolve  
(incoherently)

$$I_i(u, v) = \kappa \iint I_g(\xi, \eta) |h(u - \xi, v - \eta)|^2 d\xi d\eta$$

Names:

Incoherent impulse response

Intensity impulse response

Point-spread function (PSF)

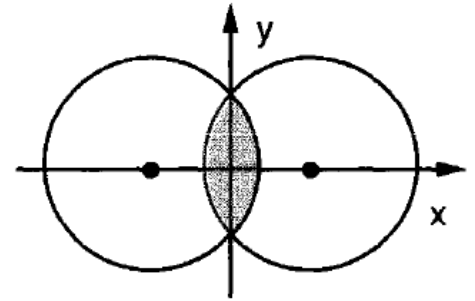
# Incoherent imaging

$$I_i(u, v) = \kappa \iint I_g(\xi, \eta) |h(u - \xi, v - \eta)|^2 d\xi d\eta$$

$$I_i(u, v) = \kappa \mathcal{F}^{-1} \left\{ \mathcal{F} \{ I_g(\xi, \eta) \} \text{OTF}(f_x, f_y) \right\}$$

$$\text{OTF}(f_x, f_y) = P(-\lambda z_i f_x, -\lambda z_i f_y) \star P(-\lambda z_i f_x, -\lambda z_i f_y) \quad \text{Optical transfer function}$$

$$\text{MTF}(f_x, f_y) = \frac{|\text{OTF}(f_x, f_y)|}{|\text{OTF}(0, 0)|} \quad \text{Modulation transfer function}$$



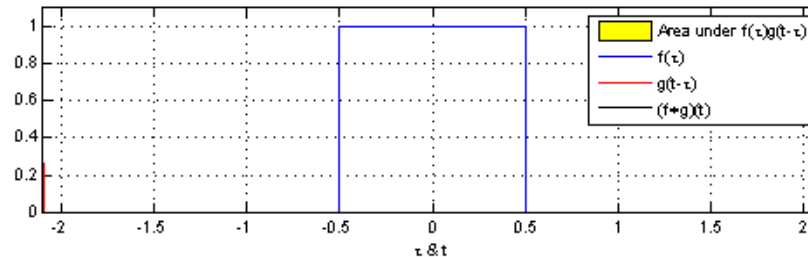
Autocorrelation  $\mathcal{F}\{|g(x, y)|^2\} = G(f_x, f_y) * G^*(-f_x, -f_y) = G(f_x, f_y) \star G(f_x, f_y)$

# Theorems of the FT

Convolution 
$$g(x, y) * h(x, y) = \iint_{-\infty}^{\infty} g(\xi, \eta)h(x - \xi, y - \eta)d\xi d\eta$$

$$\mathcal{F}\{g(x, y) * h(x, y)\} = G(f_x, f_y)H(f_x, f_y)$$

Sifting property 
$$g(x, y) * \delta(x - a, y - b) = g(x - a, y - b)$$



J. W. Goodman, Introduction to Fourier Optics, fourth edition. McMillan learning (2017)

[https://en.wikipedia.org/wiki/Convolution#/media/File:Convolution\\_of\\_box\\_signal\\_with\\_itself2.gif](https://en.wikipedia.org/wiki/Convolution#/media/File:Convolution_of_box_signal_with_itself2.gif)

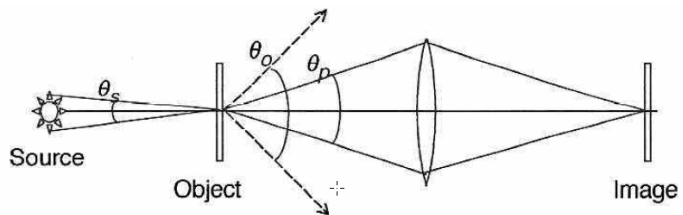
Matlab "imfilter.m" documentation

# Coherent vs incoherent imaging

Coherent

$$I_i(u, v) = \left| \iint U_g(\xi, \eta) h(u - \xi, v - \eta) d\xi d\eta \right|^2$$

$$U_i(x, y) = \mathcal{F}^{-1} \left\{ \mathcal{F} \{ U_g(x, y) \} P(-\lambda z_i f_x, -\lambda z_i f_y) \right\}$$



Coherent if  $\theta_s \ll \theta_p$

Incoherent if  $\theta_s \geq \theta_o + \theta_p$

Partially coherent in-between

Incoherent

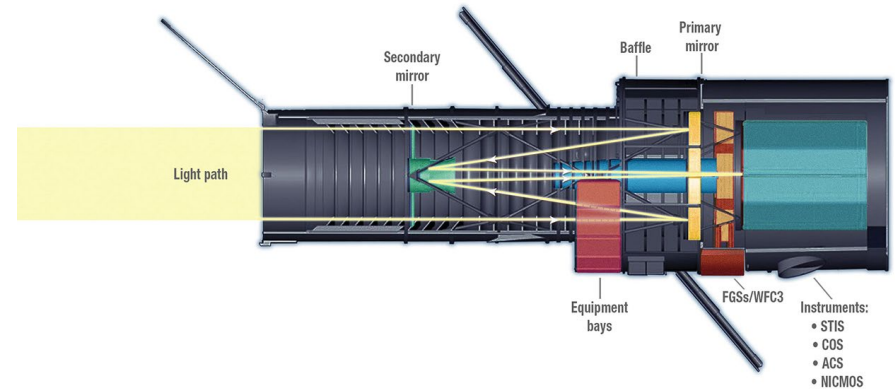
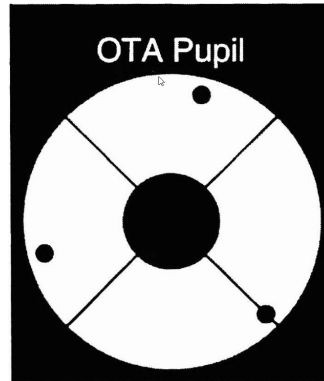
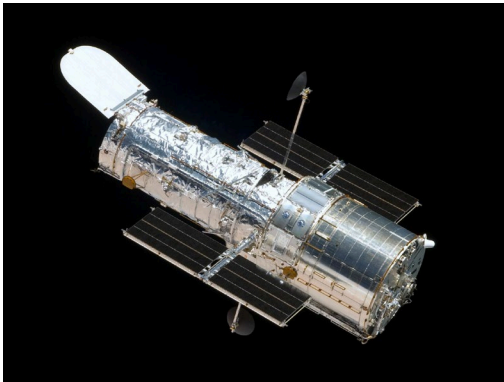
$$I_i(u, v) = \kappa \iint I_g(\xi, \eta) |h(u - \xi, v - \eta)|^2 d\xi d\eta$$

$$I_i(u, v) = \kappa \mathcal{F}^{-1} \left\{ \mathcal{F} \{ I_g(\xi, \eta) \} OTF(f_x, f_y) \right\}$$

$$OTF(f_x, f_y) = P(-\lambda z_i f_x, -\lambda z_i f_y) \star P(-\lambda z_i f_x, -\lambda z_i f_y)$$

# Telescope pupils

## Hubble space telescope



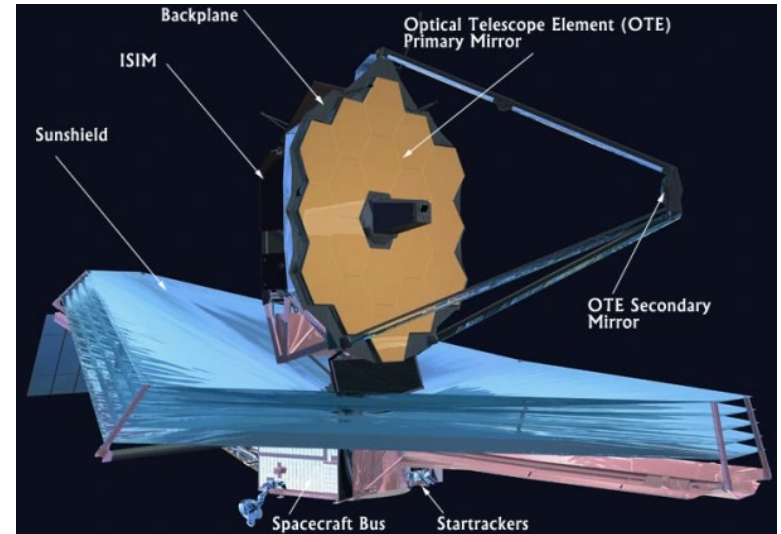
[https://en.wikipedia.org/wiki/Hubble\\_Space\\_Telescope](https://en.wikipedia.org/wiki/Hubble_Space_Telescope)

<https://hubblesite.org/contents/media/images/4520-Image.html?Tag=Hubble%20Mission>

M. Robberto et al. «Performance of HST as an infrared telescope» SPIE Proc. **4013**, UV, Optical, and IR Space Telescopes and Instruments (2000)

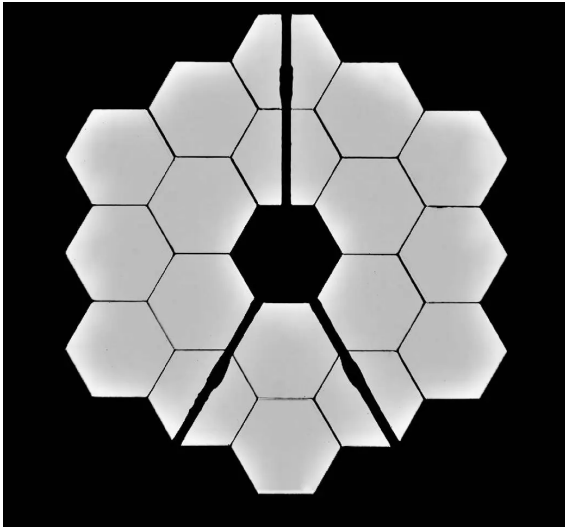
# Telescope pupils

## JWST



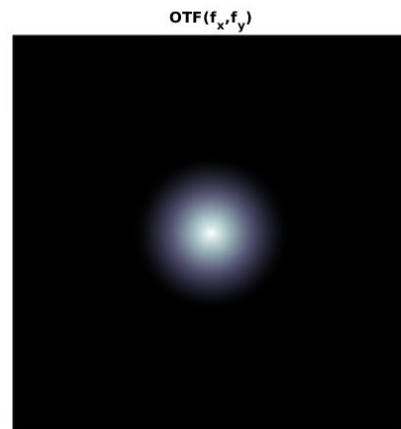
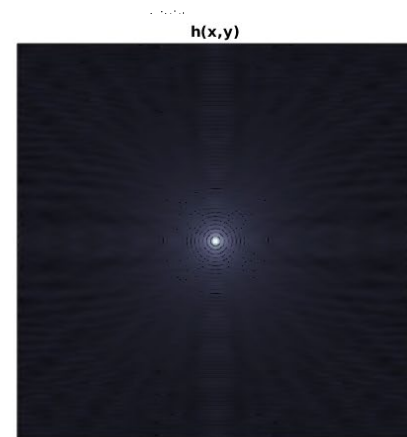
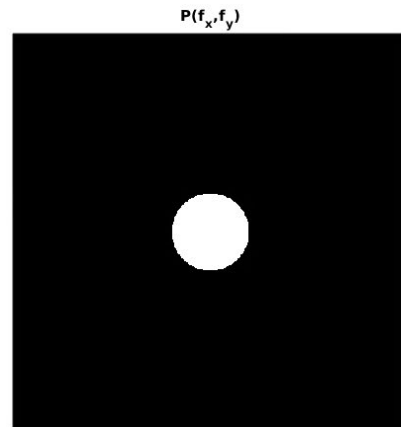
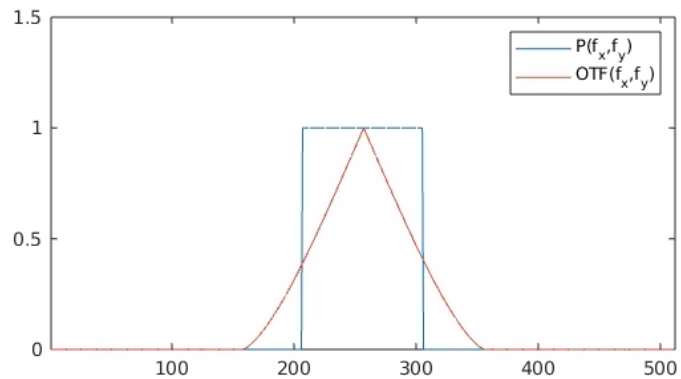
<https://spacenews.com/jwst-undamaged-from-payload-processing-incident/>  
<https://astrobit.es.org/guides/guide-to-major-telescopes/the-james-webb-space-telescope/>

# The JWST point spread function

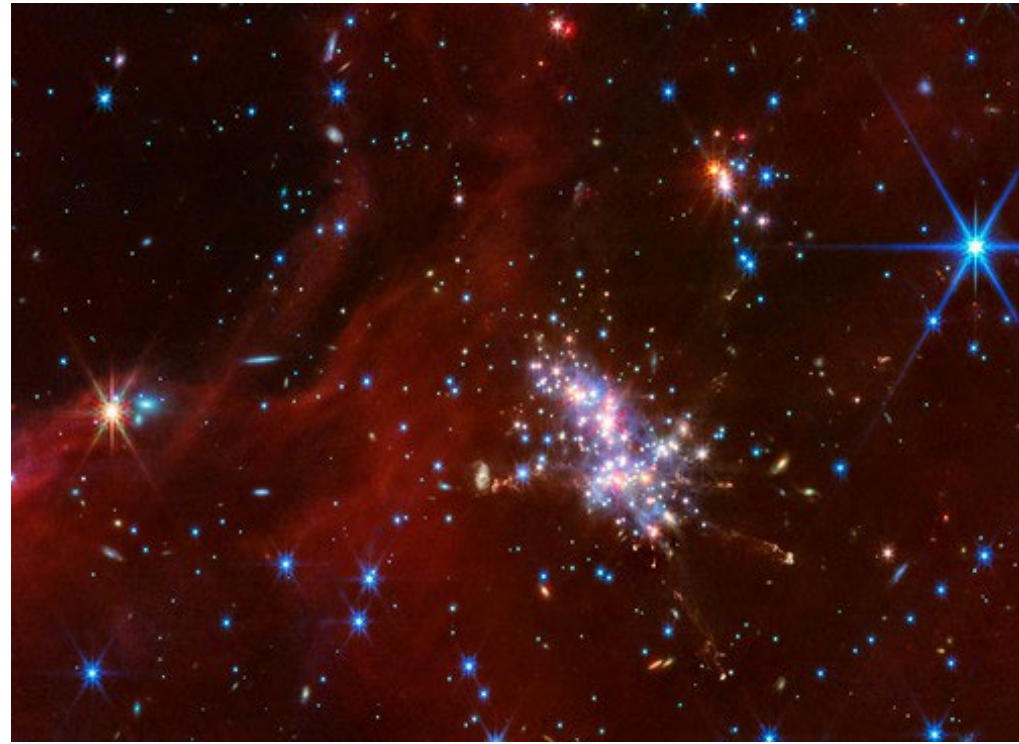
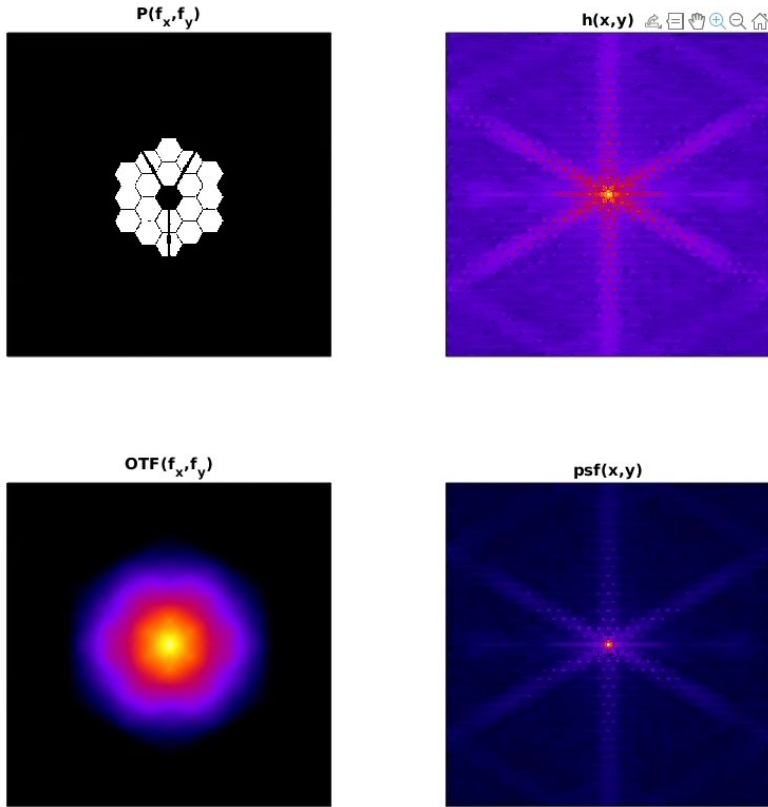


# Demonstration of different types of PSFs

[OTF\\_psf.m](#)

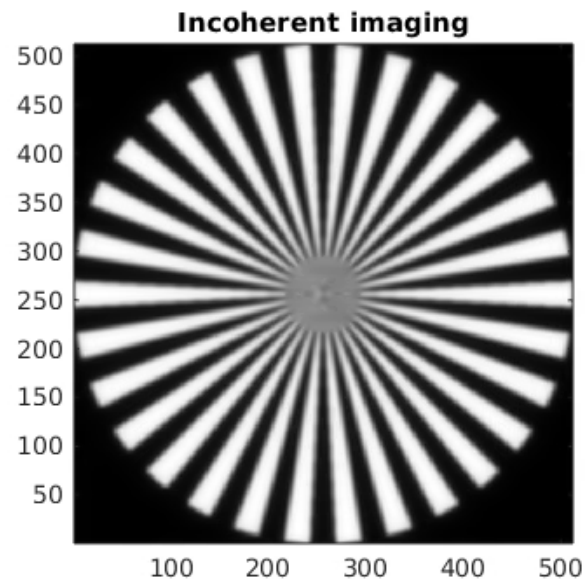
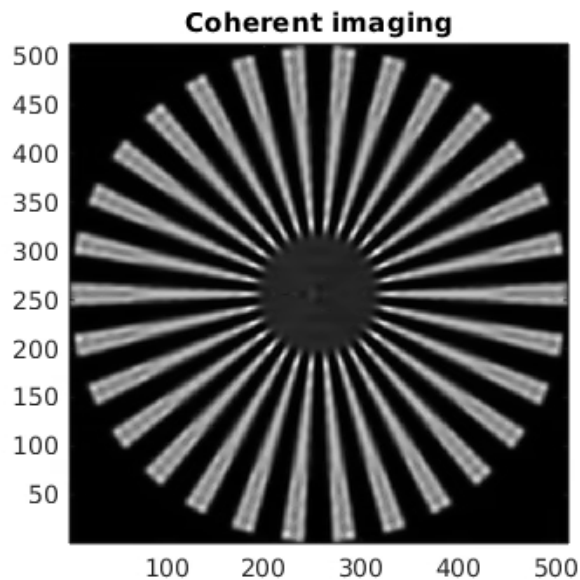
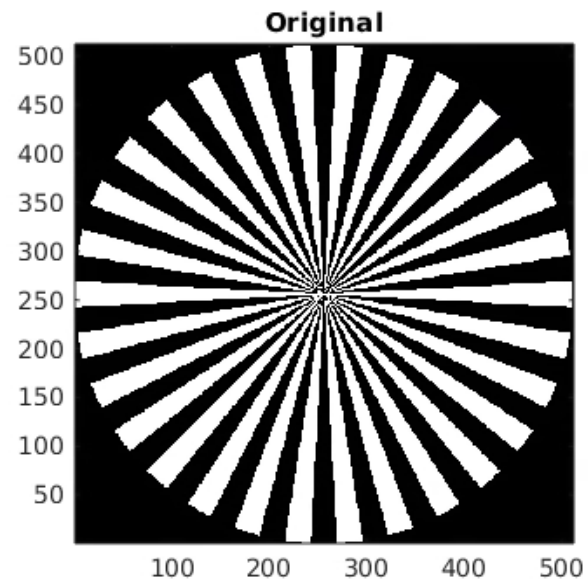
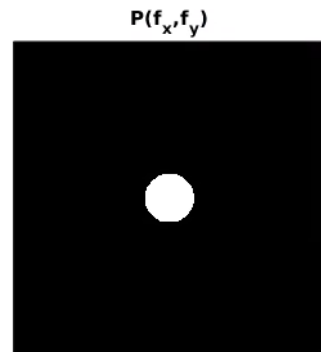
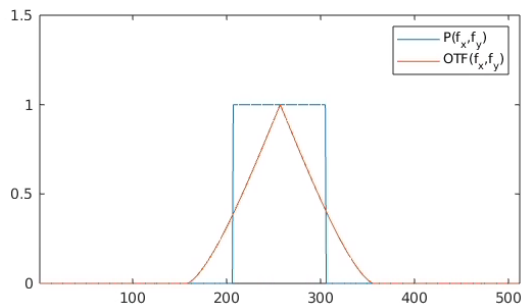


# The JWST point spread function



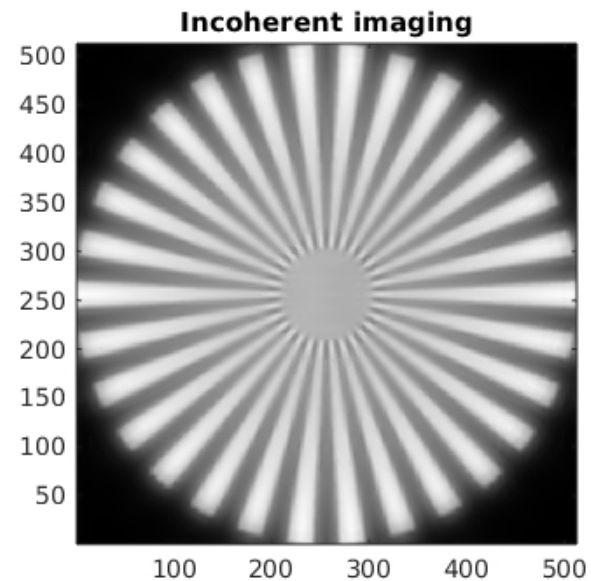
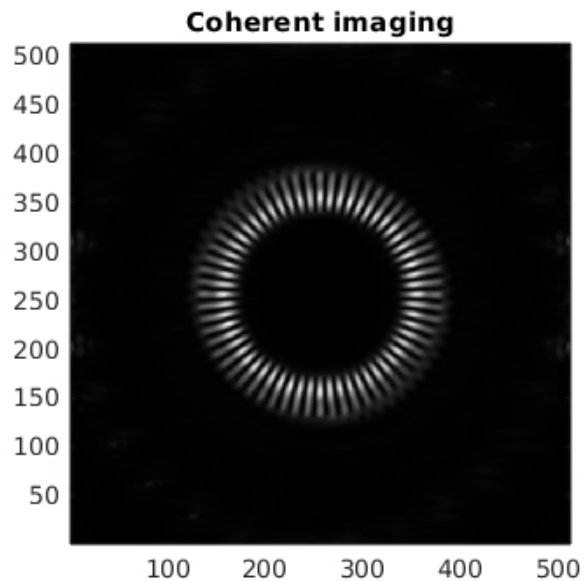
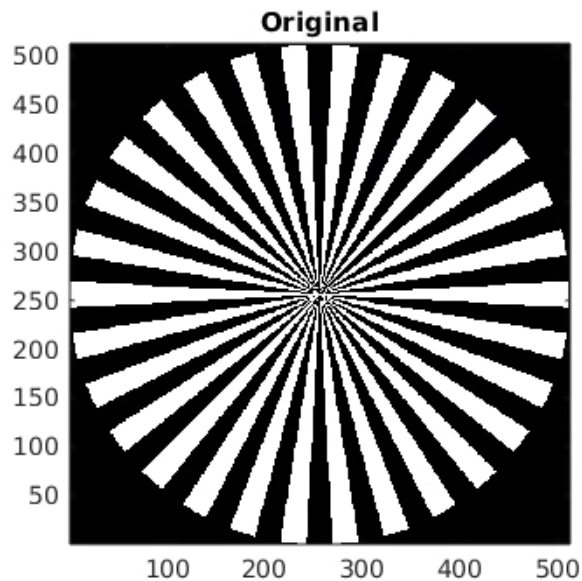
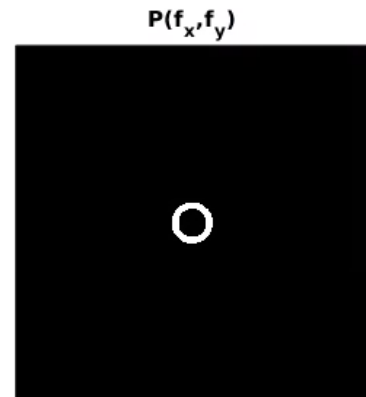
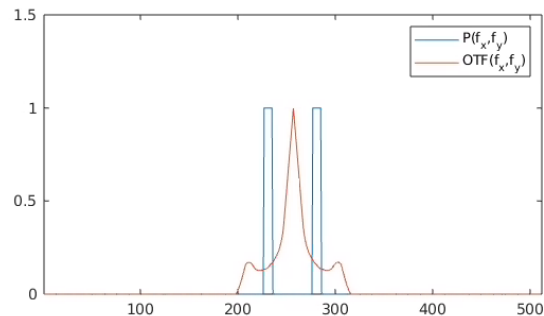
# Coherent vs incoherent imaging

OTF\_psf.m  
(with images)



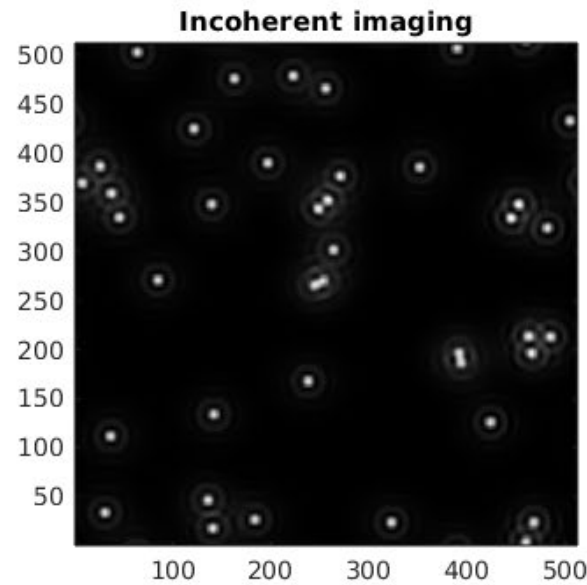
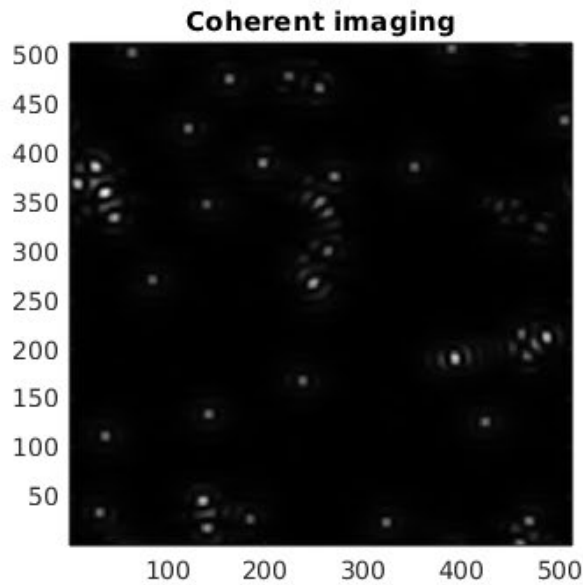
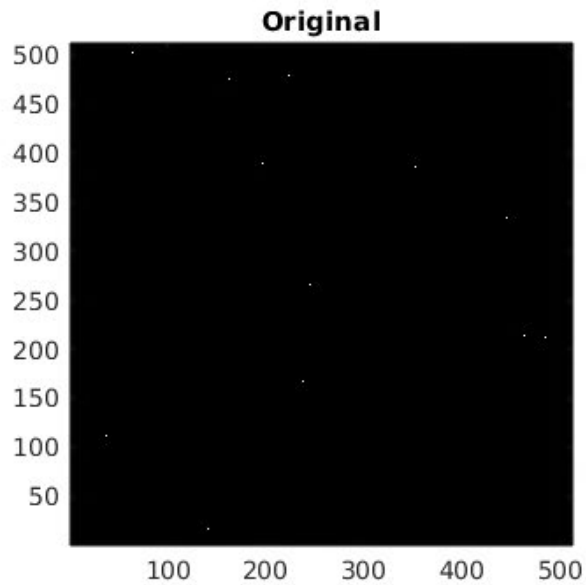
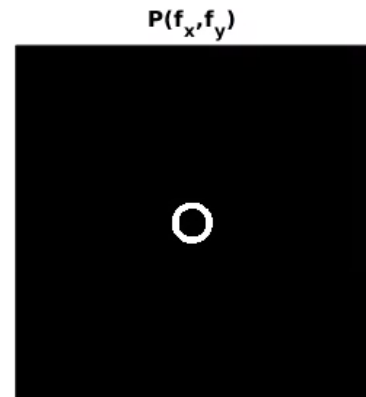
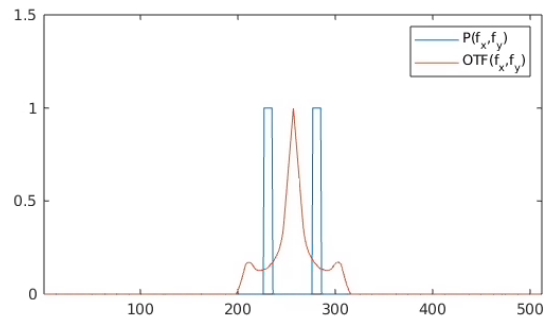
# Coherent vs incoherent imaging

OTF\_psf.m  
(with images)

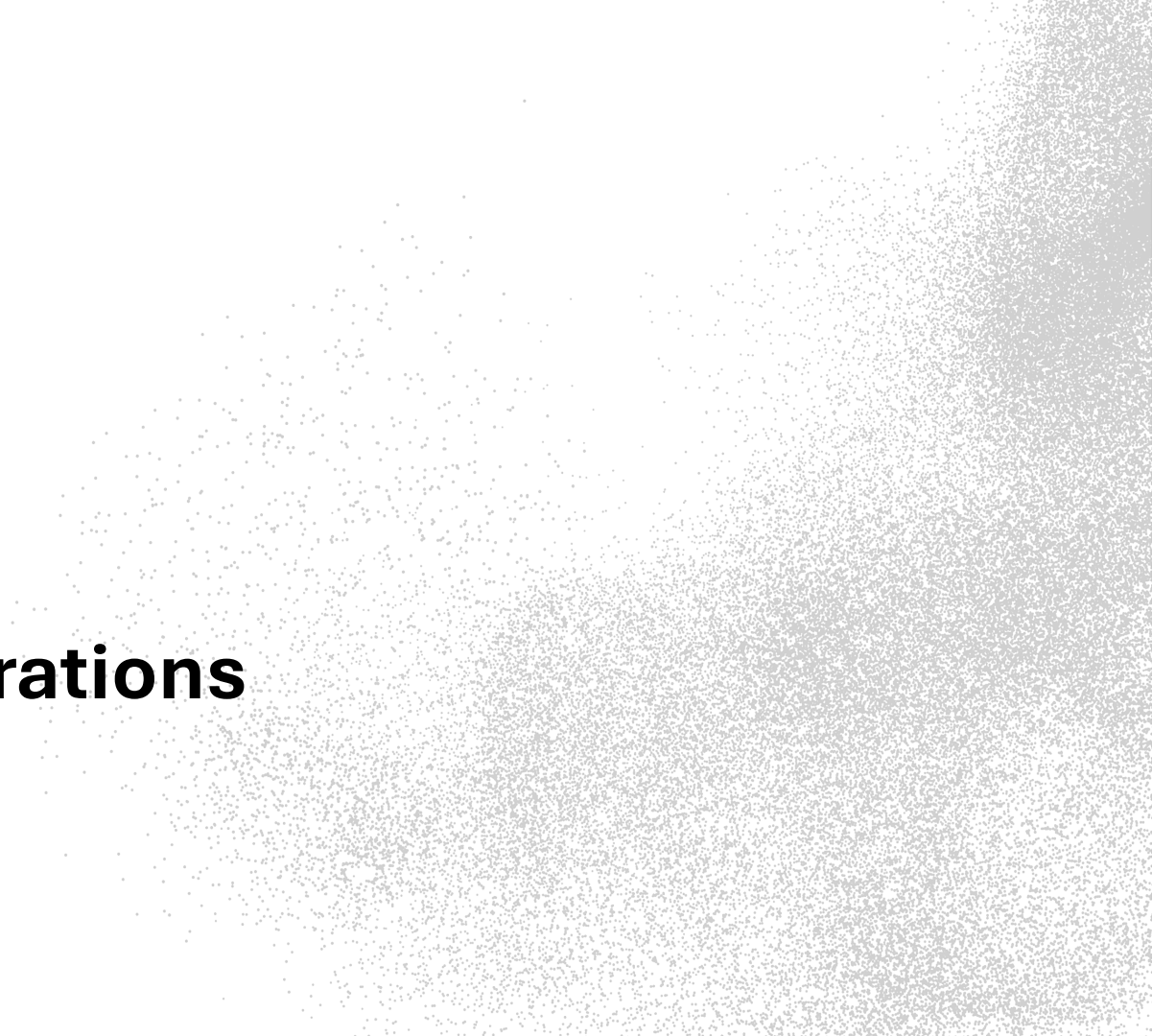


# Coherent vs incoherent imaging

OTF\_psf.m  
(with images)



# Wavefront aberrations



# Wavefront aberrations

Perfect spherical wavefront → diffraction limited

Wavefront aberrations → Deviation from perfect spherical wavefront

→ Phase error in the exit pupil

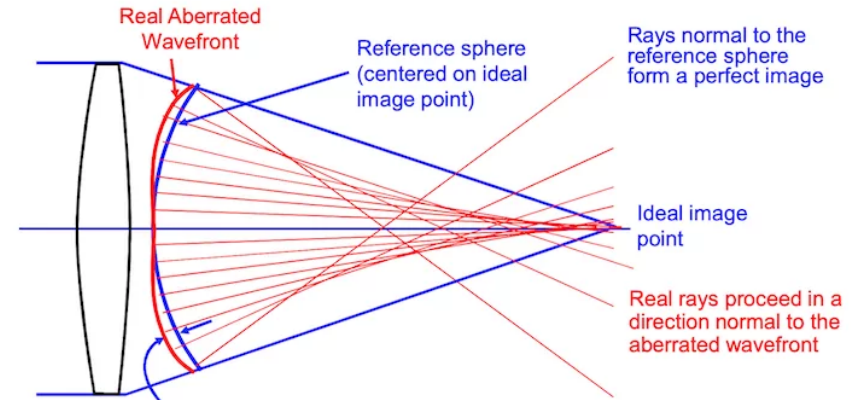
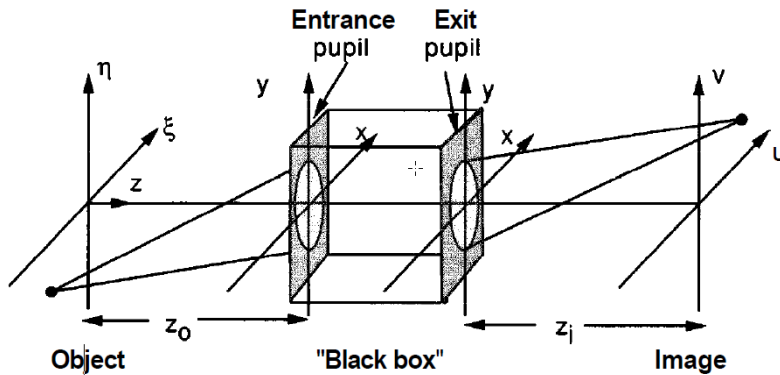
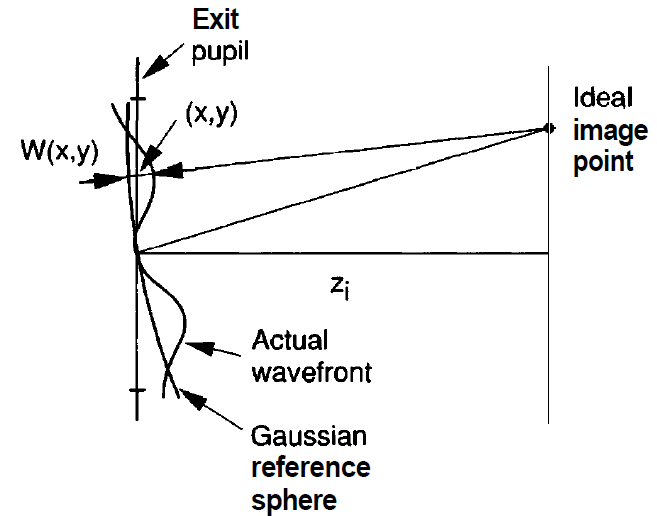


FIGURE 6.1  
Generalized model of an imaging system.

# Wavefront aberrations

Aberrations due to

- Optical design
- Manufacturing errors
- Aberrating media (e.g. turbulence)
- Thermal stresses
- etc



Generalized pupil function (complex valued)

$$\hat{P}(x, y) = P(x, y) \exp[ikW(x, y)]$$

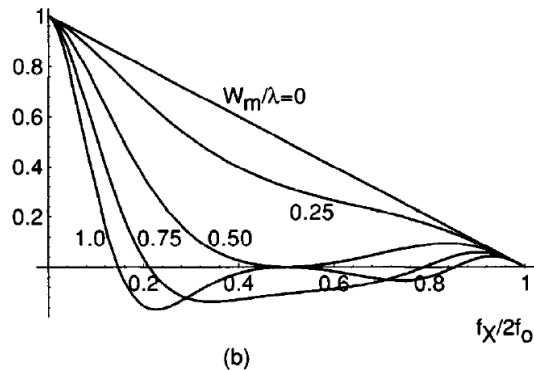
Coherent transfer function

$$H(f_x, f_y) = \hat{P}(\lambda z_i f_x, \lambda z_i f_y)$$

# Wavefront aberrations

Always reduces contrast on the OTF  $\rightarrow$  for each frequency  
Can cause contrast reversal

$$OTF(f_x, f_y) = P(-\lambda z_i f_x, -\lambda z_i f_y) \star P(-\lambda z_i f_x, -\lambda z_i f_y)$$



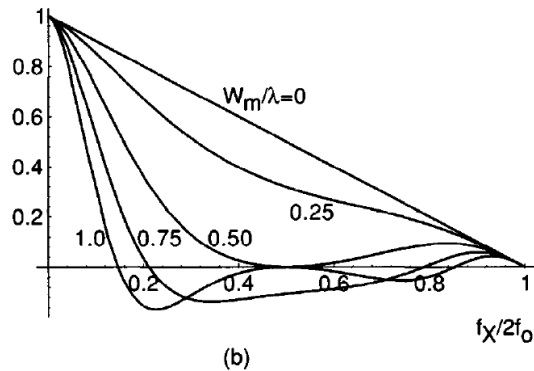
**FIGURE 6.11**  
OTF for a focusing error in a system with a square pupil. (a) Three-dimensional plot with  $f_x/2f_o$  along one axis and  $W_m/\lambda$  along the other axis. (b) Cross section along the  $f_x$  axis with  $W_m/\lambda$  as a parameter.

# Defocus aberration

Gradual attenuation of contrast wrt frequency

OTF = 0 those frequencies don't make it through

OTF < 0 contrast reversal



Maximum number of waves of OPD  $W_m / \lambda$

**FIGURE 6.11**  
OTF for a focusing error in a system with a square pupil. (a) Three-dimensional plot with  $f_x/2f_o$  along one axis and  $W_m/\lambda$  along the other axis. (b) Cross section along the  $f_x$  axis with  $W_m/\lambda$  as a parameter.

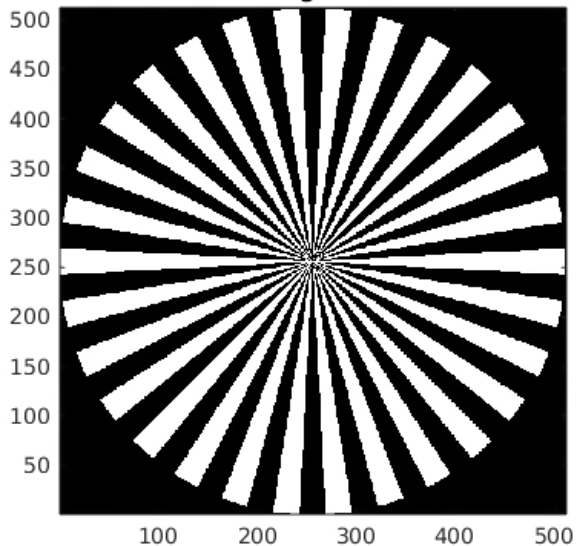
# Showing defocus of a Siemens star to see contrast reversal

```
%% Pupil %%  
masktype = 'circle'; % circle, ring, jwst  
Nmask = 70; % Circle diameter  
ring_ratio = 1.5; % R1/R2 for ring  
N = 512;
```

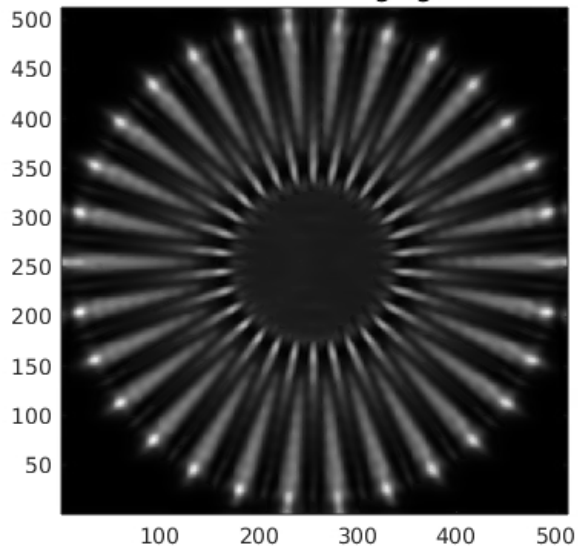
```
%% Image %%  
image_type = 'spokes'; % spokes, stars, cameraman  
num_spokes = 15;  
num_stars = 40;  
show_image = true;
```

```
%% Aberrations %%  
defocus = 0.9; % wave  
show_aberrations = 1;
```

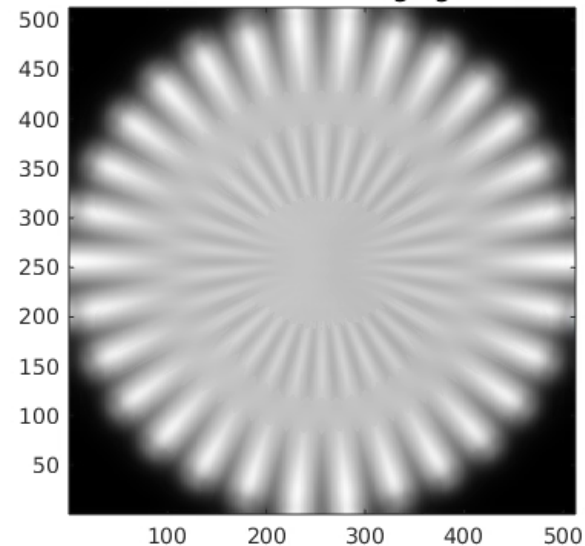
Original

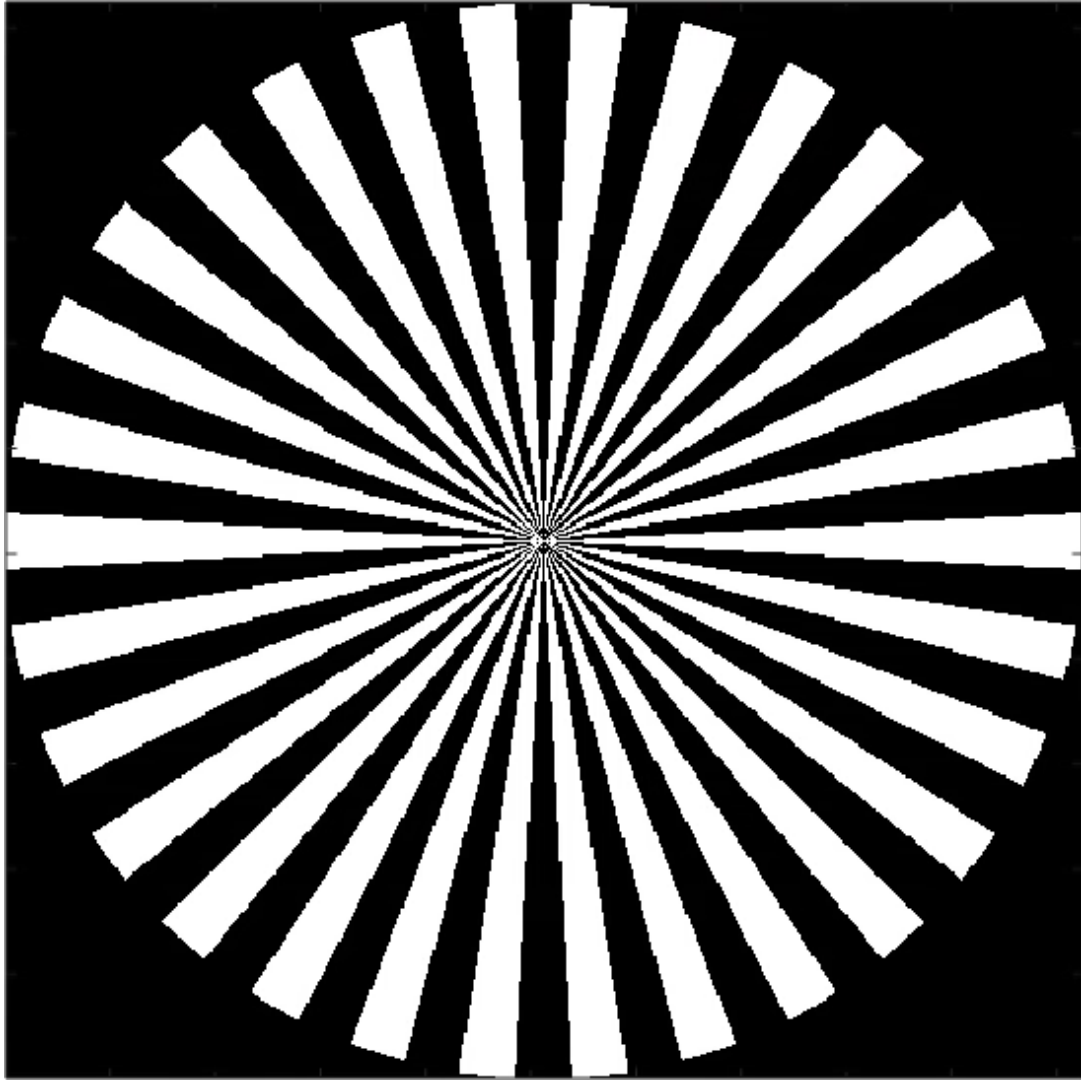


Coherent imaging



Incoherent imaging







# Diffraction limited

Imaging performance limited by diffraction, not by aberrations

**Maréchal criterion.** Formally, that a wavefront can be regarded as diffraction-limited if its RMS phase error is 14 times less than its wavelength.

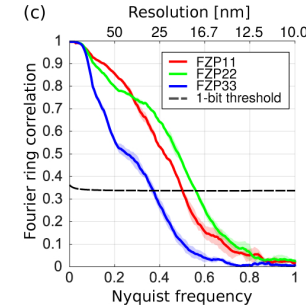
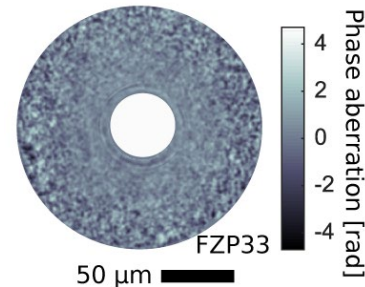
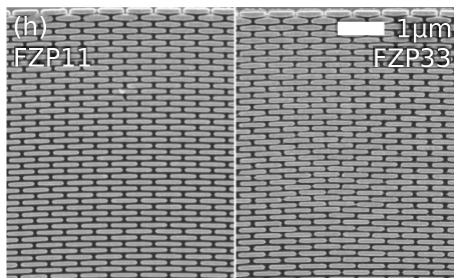
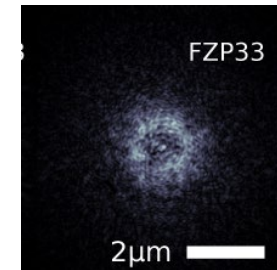
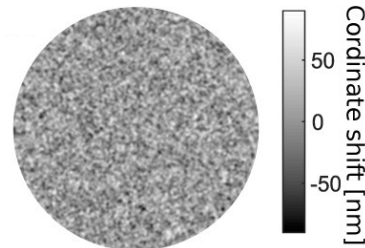
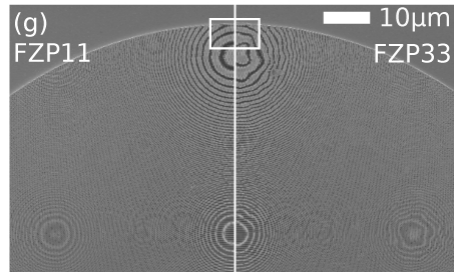
$$\sigma_w < \frac{\lambda}{14} \approx 0.071\lambda$$

**Strehl ratio.** PSF peak intensity / ideal PSF peak intensity  
 $S > 0.8$  is considered diffraction limited

$$S = \frac{|h_{\max}|^2}{|h_{\text{perfect,max}}|^2} = \left| \langle \exp(ikW) \rangle \right|^2 \approx \exp(-k^2 \sigma_w^2)$$

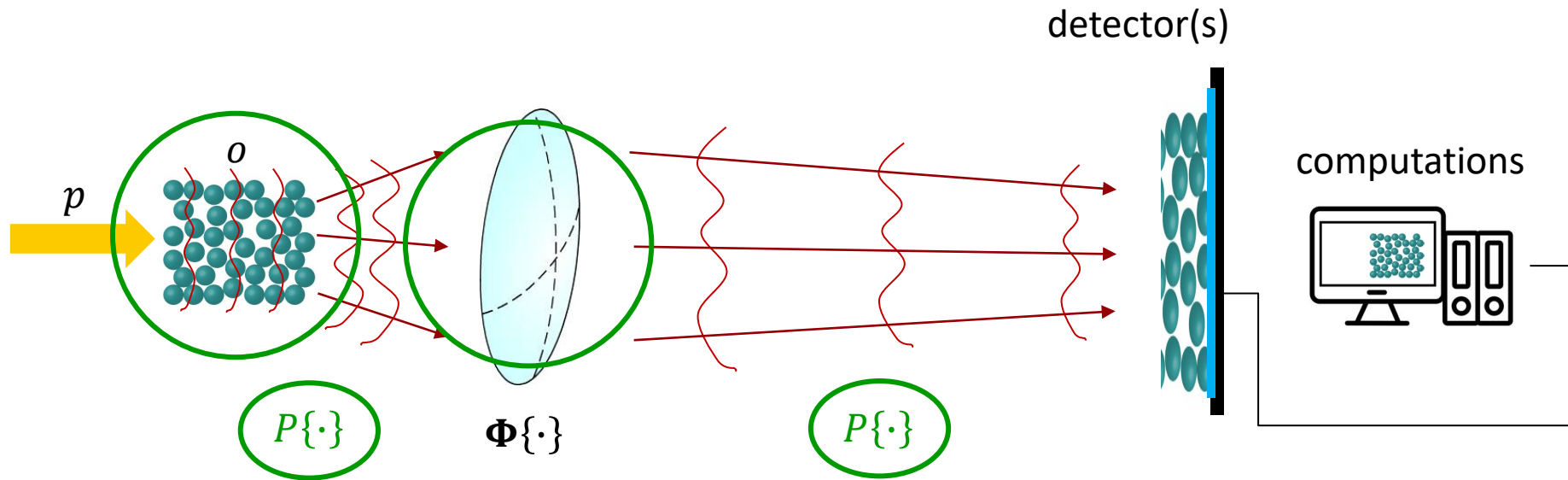
# Ugly lenses – engineered distortions for ptychography

We introduce engineered wavefront distortions to introduce structure in the beam and increase diversity in the datasets



# Lenses and imaging

A more detailed model



**Move to Chapter 3**